

Thermal- compositional- reactive simulation with DARTS

Denis Voskov



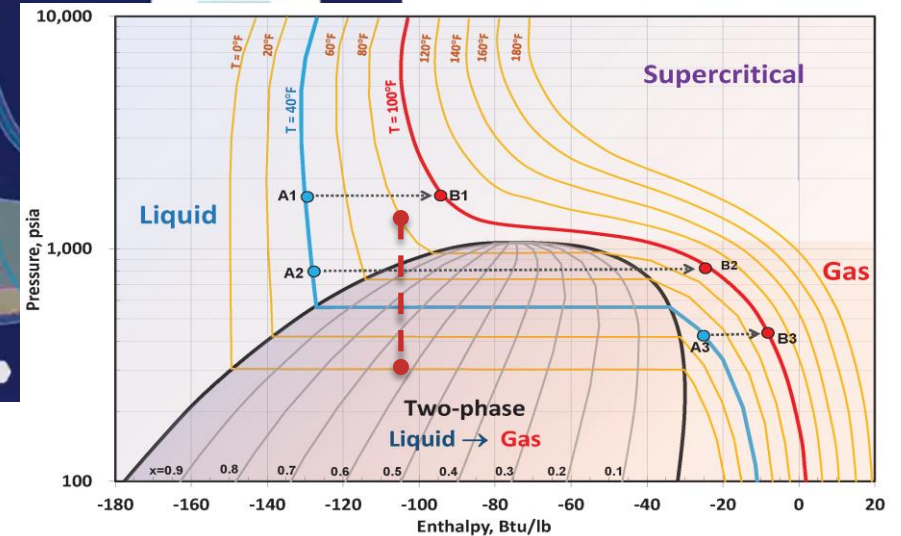
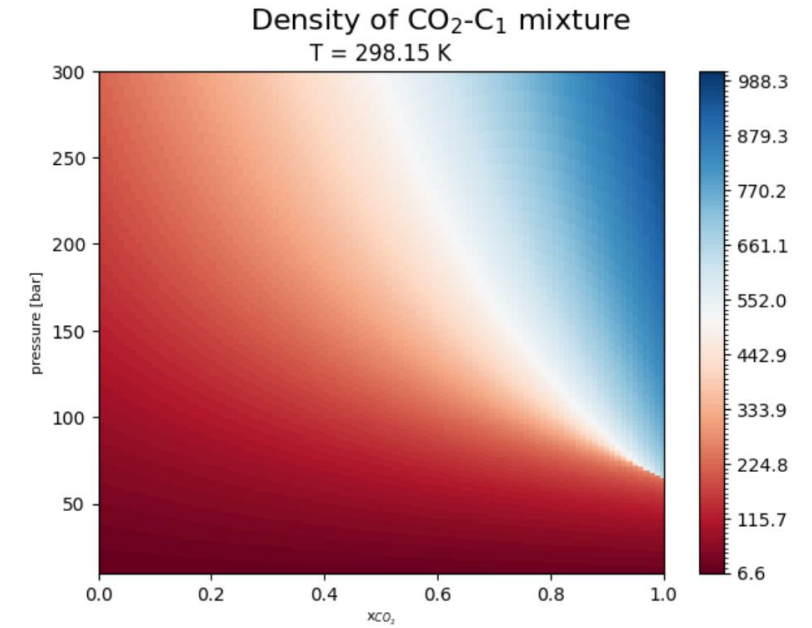
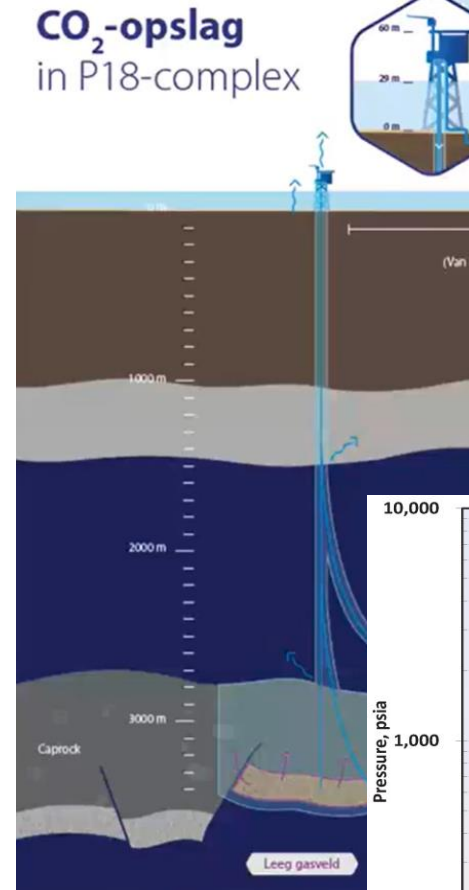
CO₂ injection into depleted fields

➤ Injection into depletion reservoir

- Pressurizing reservoir
- Joule-Thomson cooling
 - Hydrate formation
- Salt precipitation
 - Capillary backflow

➤ Injectivity interruption

- Pressure depletion
- Two-phase cooling
 - Hydrate formation

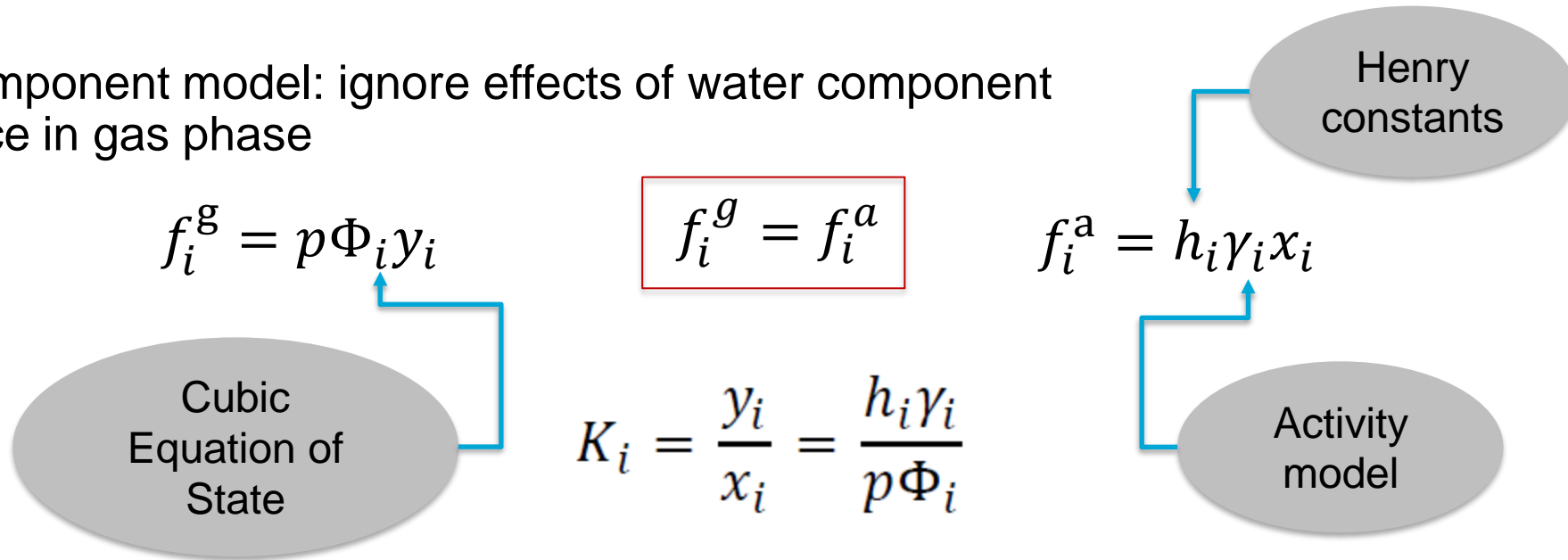


Challenge with CO2 expansion



Thermodynamics of CO₂-gas-brine

- Gas component model: ignore effects of water component presence in gas phase



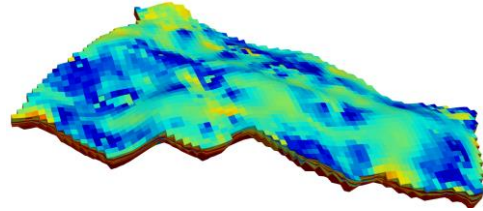
- Derive enthalpy directly from EoS for gas, liquid and aqueous phases

$$h^g = -RT^2 \sum n_i \left(\frac{\partial \ln \phi_i}{\partial T} \right), \quad h^a = -RT^2 \sum n_i \left(\frac{\partial \ln \gamma_i}{\partial T} \right)$$

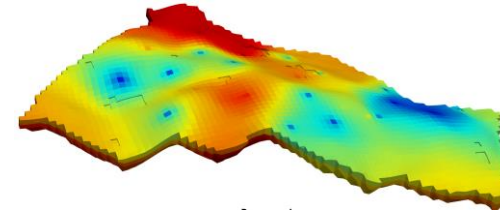
PDE for Energy Transition applications

$$\mathbf{g}(\boldsymbol{\omega}) = \mathbf{a}_t(\boldsymbol{\omega}, \boldsymbol{\xi}) + \nabla \cdot \mathbf{b}(\boldsymbol{\omega}, \boldsymbol{\xi}) + \Delta \mathbf{c}(\boldsymbol{\omega}, \boldsymbol{\xi}) + \mathbf{d}(\boldsymbol{\omega}, \boldsymbol{\xi}) = 0$$

$$\boldsymbol{\xi} = \{G, \phi_0, K_0\}$$



$$\boldsymbol{\omega} = \{p, H, z\}$$



Compressibility,
phase change
and convection

$$\mathbf{g}(\boldsymbol{\omega}) = \frac{\phi_0 V}{\Delta t} [\boldsymbol{\alpha}(\boldsymbol{\omega}) - \boldsymbol{\alpha}(\boldsymbol{\omega}_n)] + \sum_l v_t^l \boldsymbol{\beta}(\boldsymbol{\omega}) = \mathbf{0}$$

$$\alpha_c(\boldsymbol{\omega}) = c(\boldsymbol{\omega}) z_c \sum_{j=1}^{n_p} \rho_j S_j,$$

$$\beta_c(\boldsymbol{\omega}) = \frac{1}{\Lambda} \sum_{j=1}^{n_p} x_{cj}^l \rho_j^l \frac{k_{rj}^l}{\mu_j^l}$$

$$\mathbf{g}(\boldsymbol{\omega}) = \frac{\phi_0 V}{\Delta t} [\boldsymbol{\alpha}(\boldsymbol{\omega}) - \boldsymbol{\alpha}(\boldsymbol{\omega}_n)] + \sum_l v_t^l \boldsymbol{\beta}(\boldsymbol{\omega}) + \sum_l \mathbf{D}^l (\boldsymbol{\chi}^l - \boldsymbol{\chi}) \boldsymbol{\gamma}(\boldsymbol{\omega}) + V \boldsymbol{\delta}(\boldsymbol{\omega}) = \mathbf{0}$$

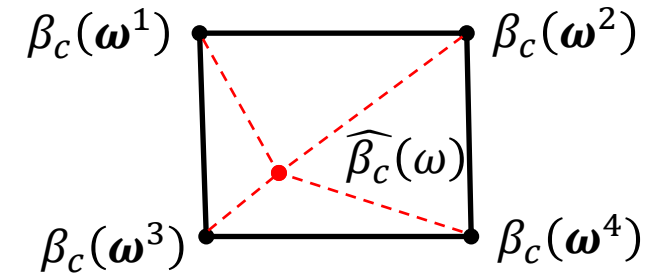
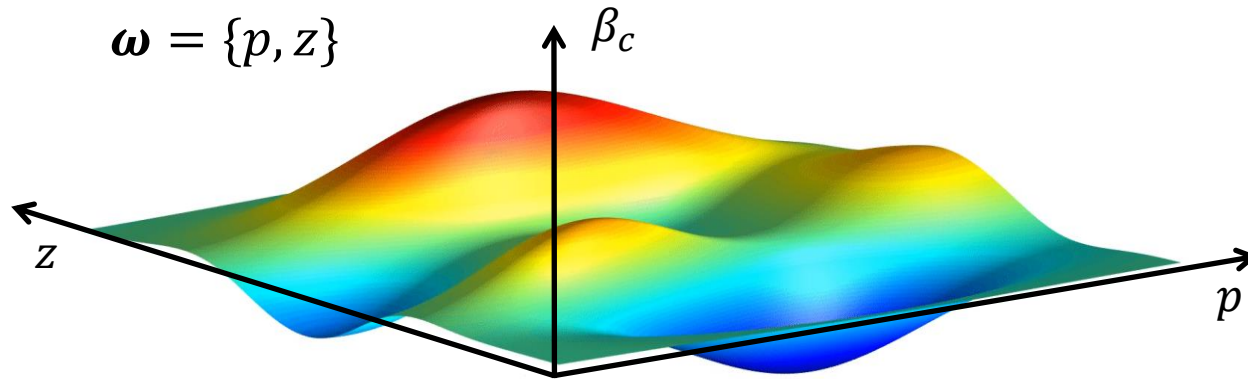
+ diffusion and
reactions

$$\gamma_c(\boldsymbol{\omega}) = c(p) \sum_{j=1}^{n_p} x_{cj} \rho_j S_j d_{cj},$$

$$\delta_c(\boldsymbol{\omega}) = \sum_{k=1}^{n_k} v_{ck} r_k$$

Operator-Based Linearization

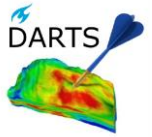
$$\beta_c(\boldsymbol{\omega}) = \frac{1}{\Lambda} \sum_{j=1}^{n_p} x_{cj}^l \rho_j^l \frac{k_{rj}^l}{\mu_j^l}$$



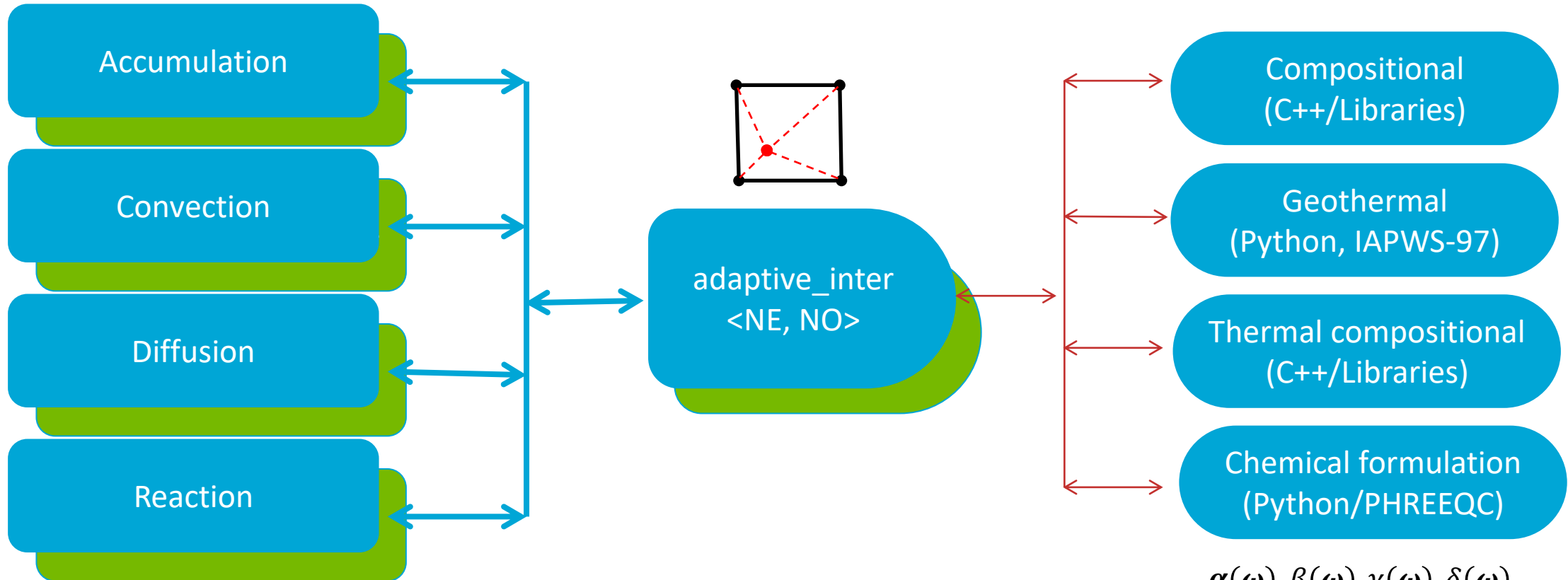
$$\frac{\partial \mathbf{g}}{\partial \boldsymbol{\omega}} = \frac{\partial \boldsymbol{\alpha}}{\partial \boldsymbol{\omega}} \bar{\mathbf{a}}(\boldsymbol{\omega}, \boldsymbol{\xi}) + \frac{\partial \boldsymbol{\beta}}{\partial \boldsymbol{\omega}} \bar{\mathbf{b}}(\boldsymbol{\omega}, \boldsymbol{\xi}) + \frac{\partial \boldsymbol{\gamma}}{\partial \boldsymbol{\omega}} \bar{\mathbf{c}}(\boldsymbol{\omega}, \boldsymbol{\xi}) + \frac{\partial \boldsymbol{\delta}}{\partial \boldsymbol{\omega}} \bar{\mathbf{d}}(\boldsymbol{\omega}, \boldsymbol{\xi}) + \bar{\mathbf{f}}(\boldsymbol{\omega}, \boldsymbol{\xi})$$

$$|\widehat{\beta}_c - \beta_c| \leq cA^2 \sup_{\boldsymbol{\omega}} |\nabla^2 \beta_c|$$

Open Delft Advanced Research Terra Simulator

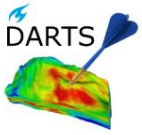


DARTS-engine: C++ & CUDA



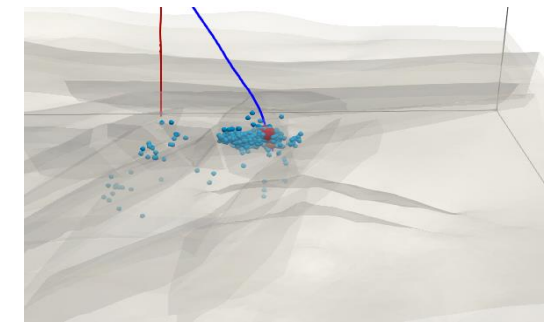
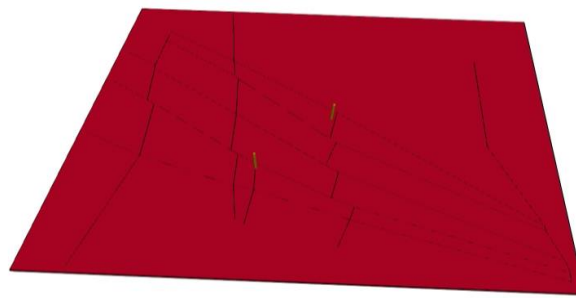
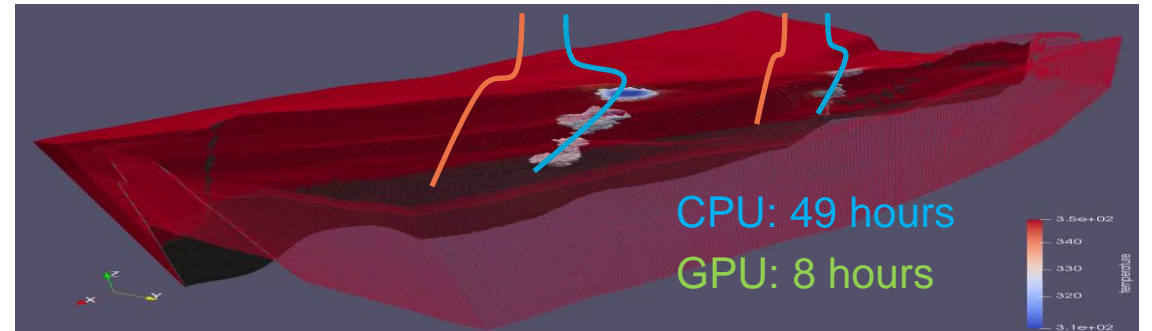
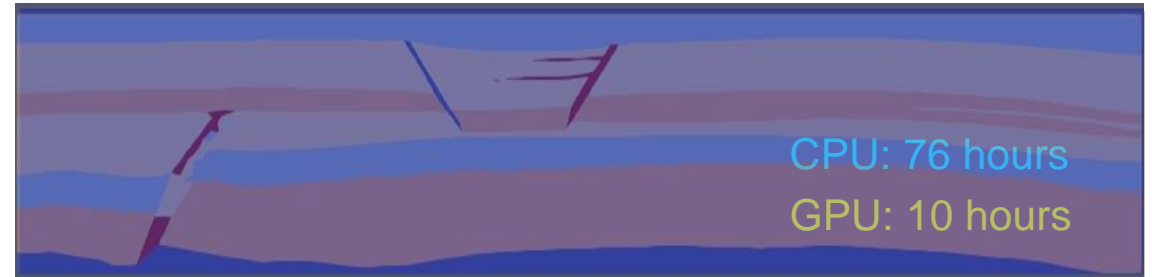
DARTS-physics: hybrid

$$\mathbf{a}_t(\omega, \xi) + \nabla \cdot \mathbf{b}(\omega, \xi) + \Delta c(\omega, \xi) + \mathbf{d}(\omega, \xi) = \mathbf{0}$$



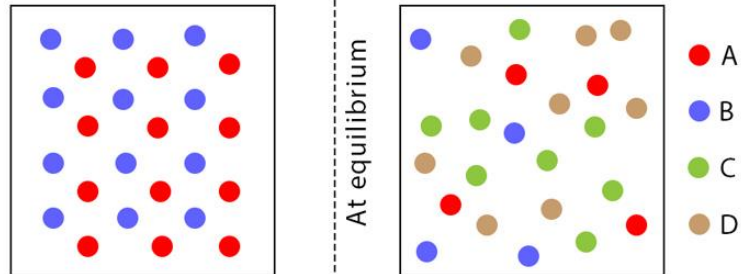
Delft Advanced Research Terra Simulator

- Operator-Based Linearization
 - Parametrization of thermodynamics
 - Adaptivity in parametrization
- Flexibility and performance
 - Flexible nonlinear physics
 - Implementation at GPU
 - Adjoint capabilities
- Complex thermodynamics
 - Thermal-compositional formulation
 - Fully coupled chemistry
 - Fully coupled geomechanics



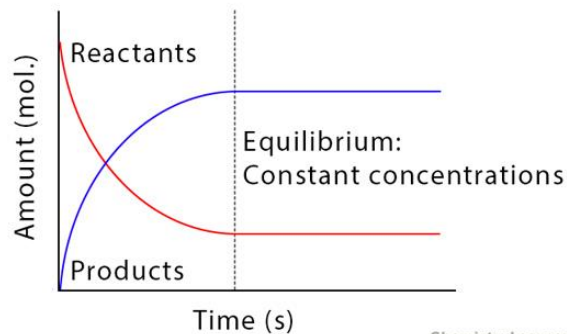
Equilibrium chemical reactions

Chemical Equilibrium with Constant Concentrations



Initial concentration of the reactants

Concentrations of reactants and products at equilibrium



ChemistryLearner.com

Component mass balance:

$$\frac{\partial}{\partial t} (\phi \rho_j z_c) + \nabla \cdot (\rho_j z_c \mathbf{u}) = \sum_{r=1}^{n_r} v_{c,r} r_r$$

$$a_c + l_c = Vr$$

$$a_c + l_c = Vr \times E \Rightarrow a_e + l_e = 0$$

$$K_{sp} - Q_{sp} = 0 \quad \text{equilibrium}$$

Chemical reactions:

$$a_c^k + l_c^k = vr^k \quad \text{kinetic}$$

Equilibrium reactions in brine-CO₂ system

$$\mathbf{E} \times \frac{\partial}{\partial t} (\phi \rho_t z_c) + \text{div}(\mathbf{l}_c) = \sum_{q=1}^{n_q} v_{cq} r_q$$

$$f_i^g = f_i^l$$



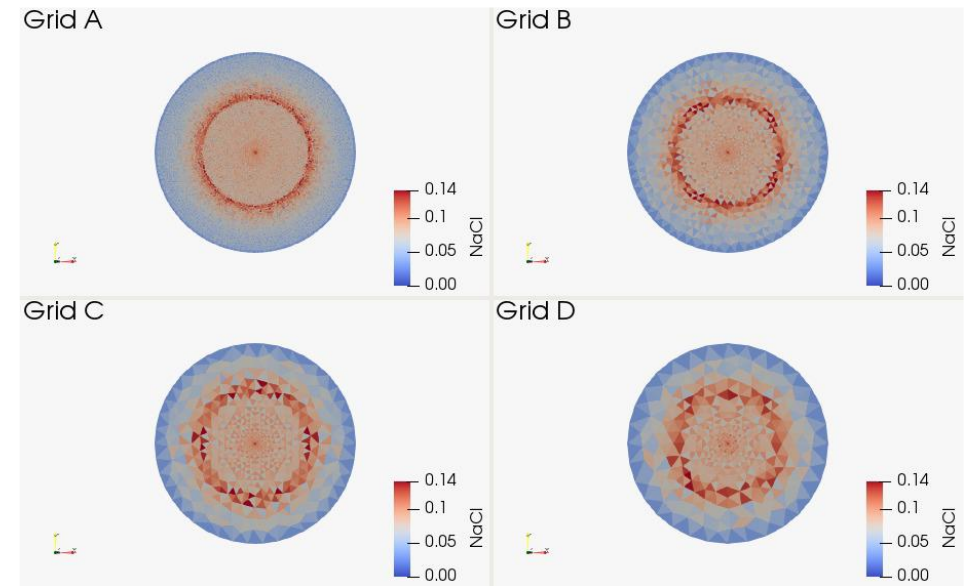
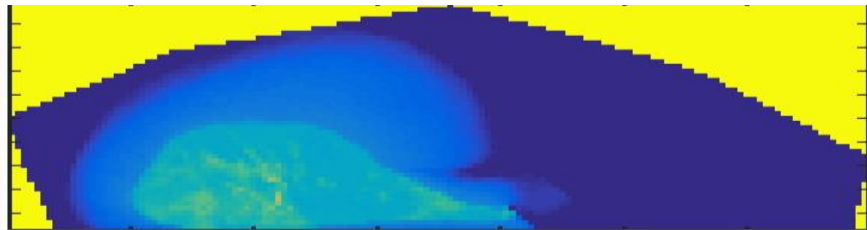
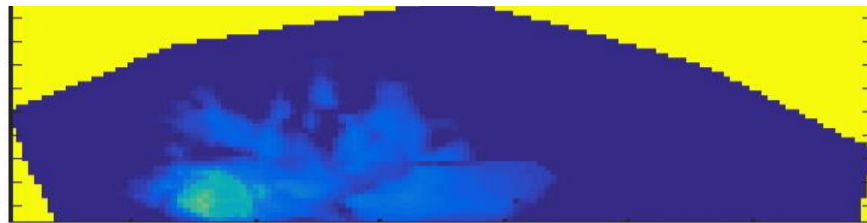
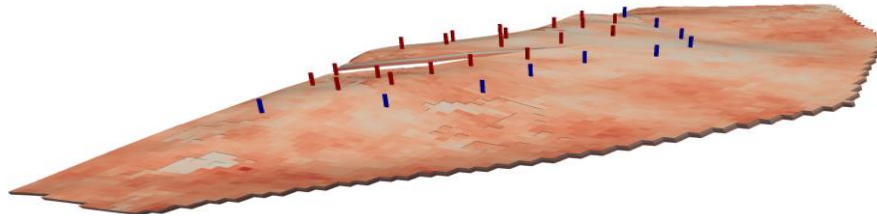
$$\frac{\partial}{\partial t} (\phi^T \rho_t^E z_i^E) + \text{div}(\mathbf{e}_i \mathbf{l}) = 0$$

$$f_i^g = f_i^l$$

$$\rho_t^E = \rho_t \sum_{i=1}^{n_e} \mathbf{e}_i z$$

$$\prod_{c=1}^{n_c} a_c^{v_{cq}} - K_q = 0$$

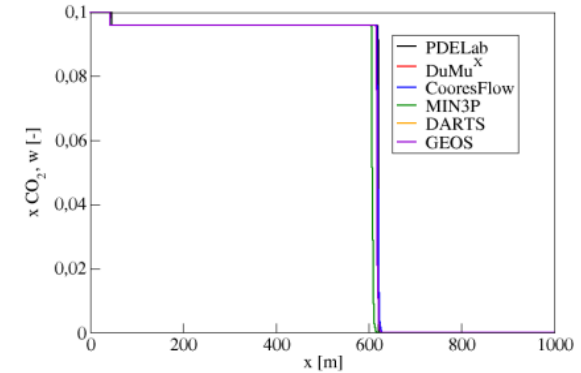
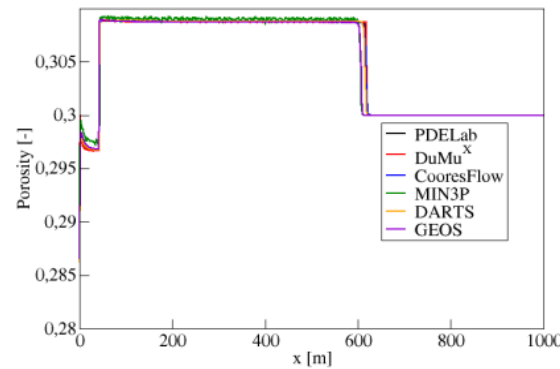
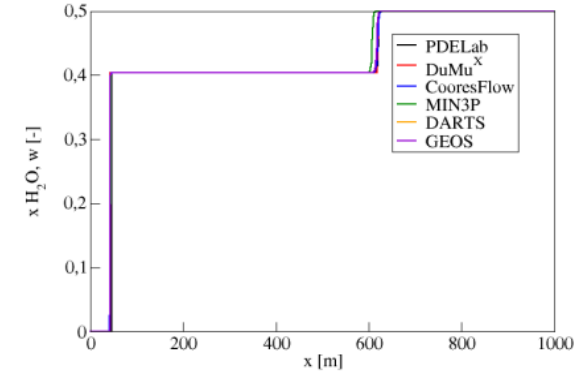
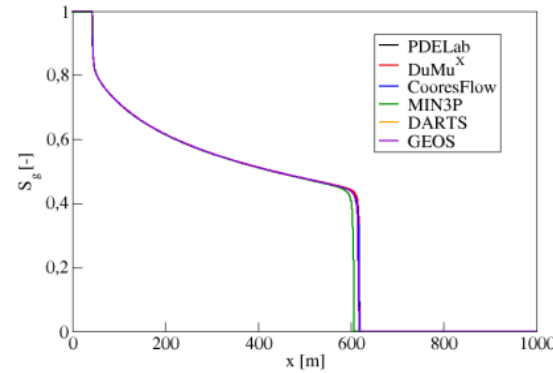
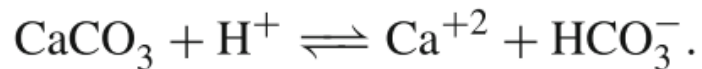
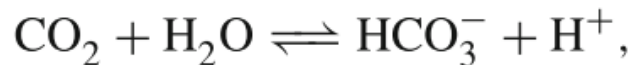
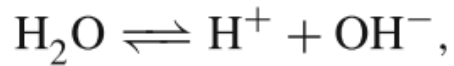
$$\mathbf{z}^E \sum_{i=1}^{n_e} \mathbf{e}_i z - \mathbf{E} z = 0$$



Multiphase flow with reactions (1D benchmark)

$$\frac{\partial n_c}{\partial t} + l_c + q_c = \sum_{k=1}^K v_{ck} r_k^K + \sum_{q=1}^Q v_{cq} r_q^Q, \quad c = 1, \dots, C + M,$$

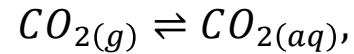
$$\phi = \phi^T \left(1 - \sum_{m=1}^M \hat{s}_m \right) \quad k = k_0 \left(\frac{\phi}{\phi_0} \right)^A$$



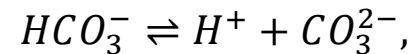
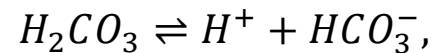
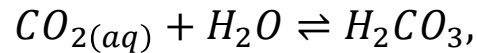
de Hoop et al., Comput. Geosci, 2024; Ahusborde et al., Comput. Geosci, 2024

CO2 injection into calcite core

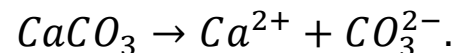
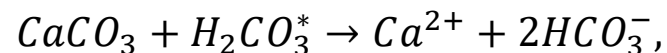
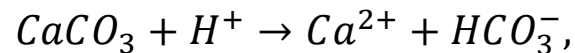
- Carbon dioxide dissolution:



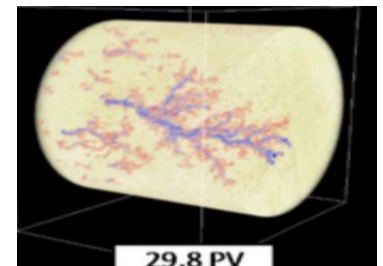
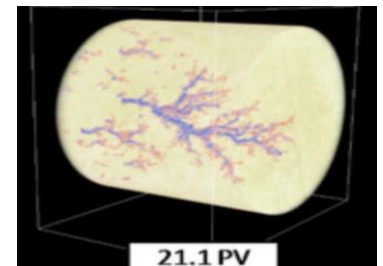
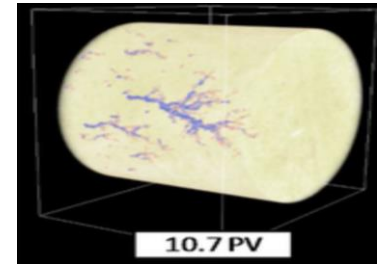
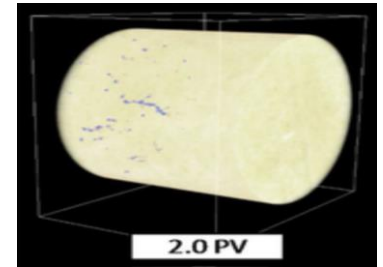
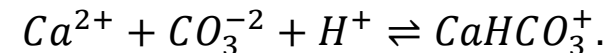
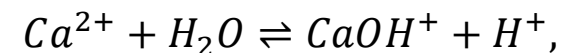
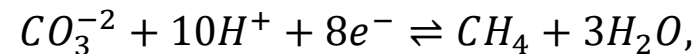
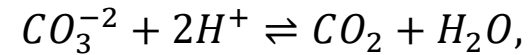
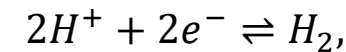
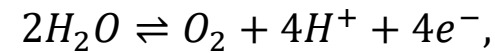
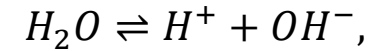
- Acid formation:



- Calcite dissolution:



- Other aqueous reactions considered:



Element balance reduction

$$\mathbf{S} = \begin{matrix} & q_1 & q_2 & q_3 & q_4 & q_5 & q_6 & k_1 \\ \begin{matrix} H_2O \\ H^+ \\ OH^- \\ CO_2 \\ HCO_3^- \\ CO_3^{2-} \\ CaCO_3 \\ Ca^{2+} \\ CaOH^+ \\ CaHCO_3^+ \\ CaCO_{3,solid} \end{matrix} & \begin{bmatrix} -1 & 0 & 1 & -1 & 0 & 0 & 0 \\ 1 & -1 & -2 & 1 & 0 & -1 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & -1 & -1 & 0 & -1 & -1 & 1 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 & -1 & -1 & 1 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & -1 \end{bmatrix} \end{matrix}$$

$$\mathbf{E} = \begin{matrix} & H_2O & H^+ & OH^- & CO_2 & HCO_3^- & CO_3^{2-} & \dots & CaCO_{3,solid} \\ \begin{matrix} H \\ O \\ C \\ Ca \\ CaCO_{3,solid} \end{matrix} & \begin{bmatrix} 2 & 1 & 1 & 0 & 1 & 0 & \dots & 0 \\ 1 & 0 & 1 & 2 & 3 & 3 & \dots & 3 \\ 0 & 0 & 0 & 1 & 1 & 1 & \dots & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & \dots & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & \dots & 1 \end{bmatrix} \end{matrix}$$

$$\mathbf{S}_{C \times R} = \left[\begin{array}{c|c} \mathbf{Q}_{Q \times K} & -\mathbf{I}_{1, Q \times Q} \\ \hline -\mathbf{I}_{2, K \times K} & \mathbf{S}_{3, K \times Q} \\ \hline \mathbf{S}_{1, (C-R) \times K} & \mathbf{S}_{2, (C-R) \times Q} \end{array} \right]$$

$$\mathbf{E}_{1(E \times C)} = \begin{bmatrix} e_{11} & e_{12} & \dots & e_{1C} \\ e_{21} & e_{22} & \dots & e_{2C} \\ \dots & \dots & \ddots & \dots \\ e_{E1} & e_{E2} & \dots & e_{EC} \end{bmatrix}$$

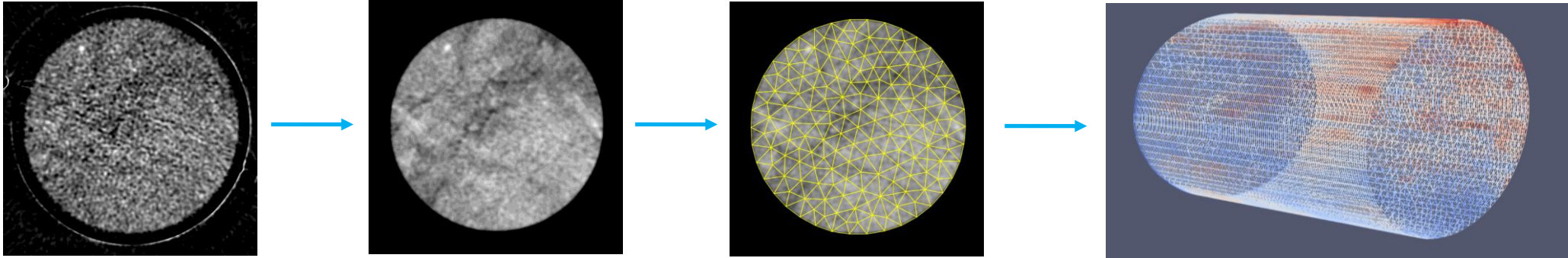
$$\mathbf{E}_{2(K \times C)} = [-\mathbf{S}_{1, K \times Q} \quad -\mathbf{I}_{2, K \times K} \quad \mathbf{0}_{K \times (C-R)}]$$

$$\frac{\partial \mathbf{n}}{\partial t} + \mathbf{1} = \mathbf{Vr},$$

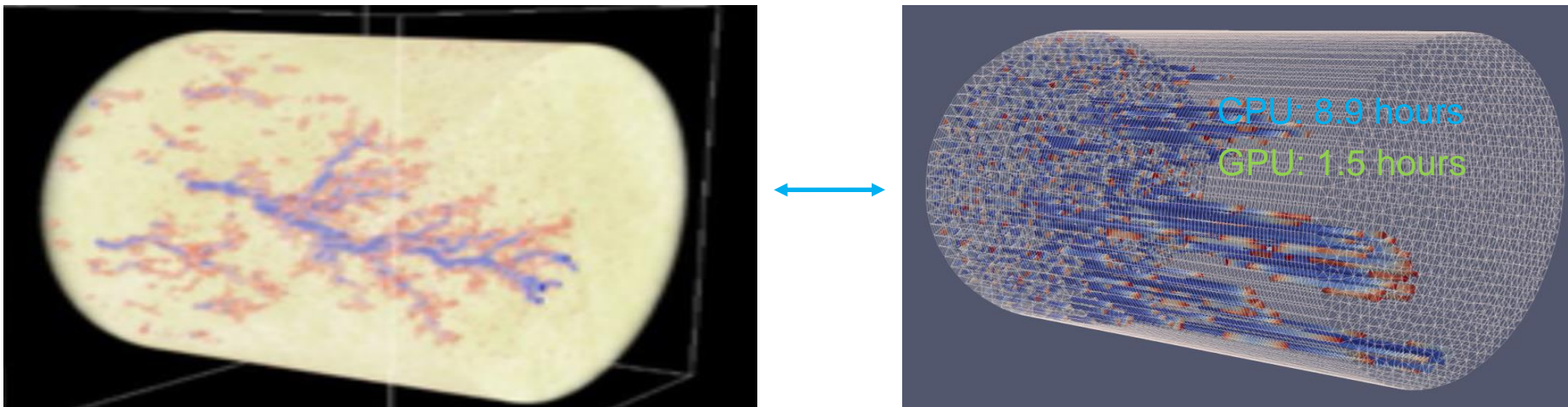
$$\frac{\partial (\mathbf{E}\mathbf{n})}{\partial t} + \mathbf{E}\mathbf{1} = \mathbf{E}\mathbf{S}\mathbf{r} = \begin{bmatrix} \mathbf{E}_1 \mathbf{S}\mathbf{r} \\ \mathbf{E}_2 \mathbf{S}\mathbf{r} \end{bmatrix} = \begin{bmatrix} 0 \\ \mathbf{r}_k \end{bmatrix}$$

Modeling of dissolution at core scale

Step 1: porosity interpretation (image subtraction, filtering, gridding)



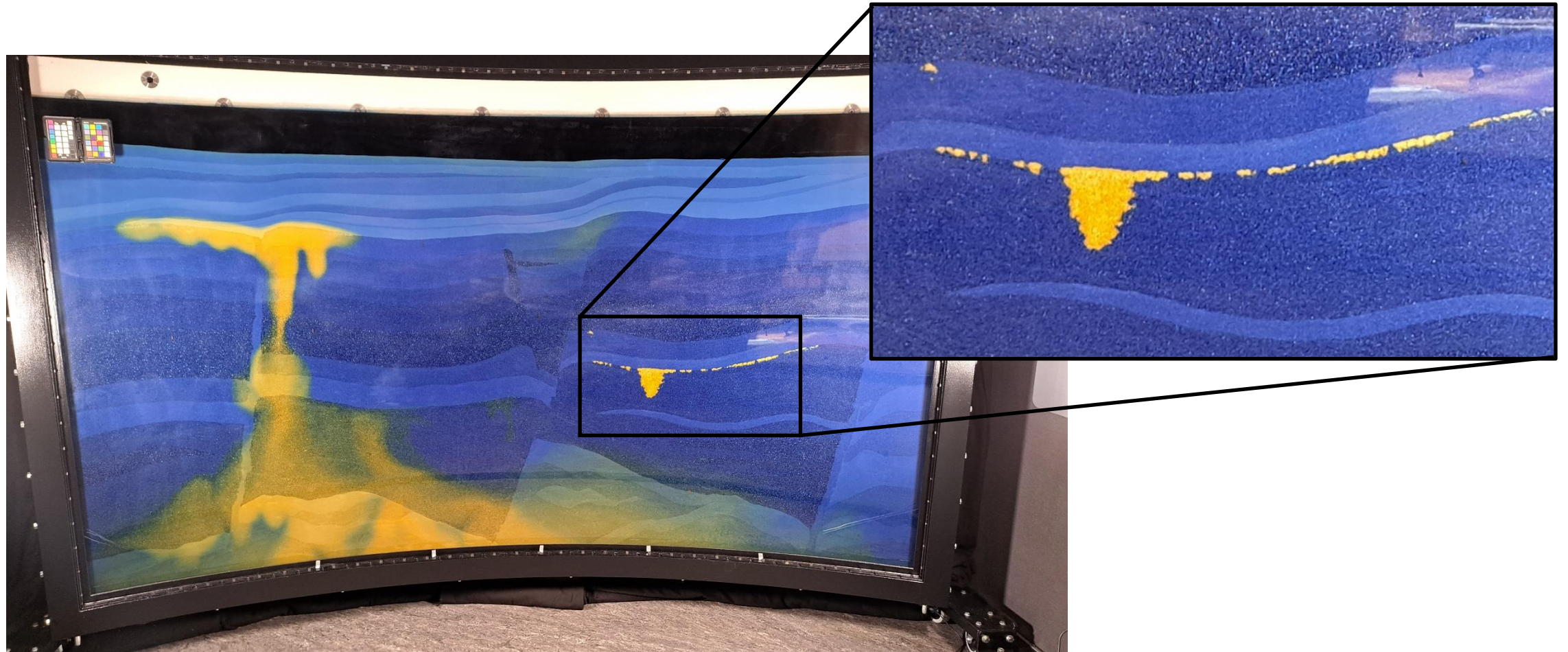
Step 2: modeling of dissolution (combination of DARTS + PHREEQC)



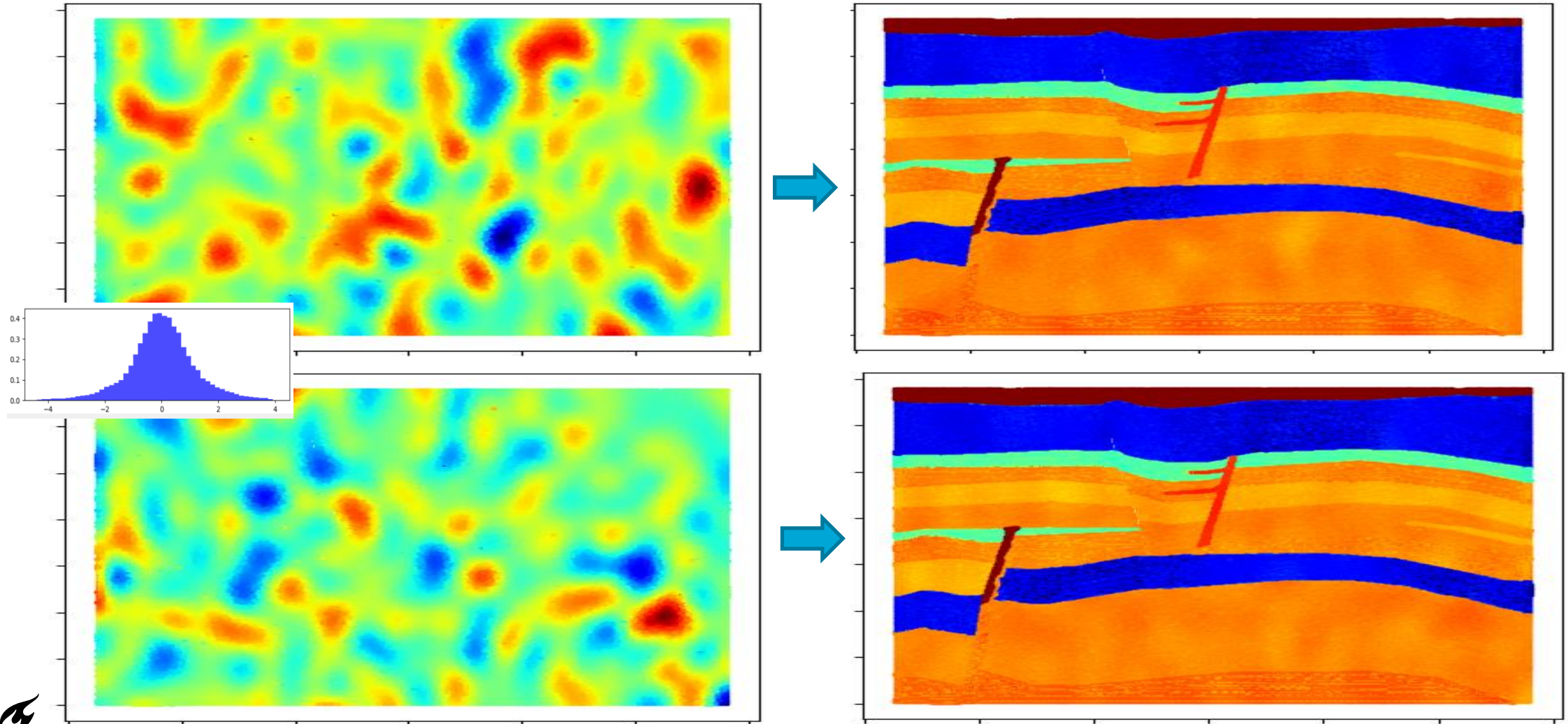
Run time:
8.9 hours (CPU engine)
PHREEQC call: 12 min

Points generated:
26068 (<0.01%)
Interpolations: 2.8e9

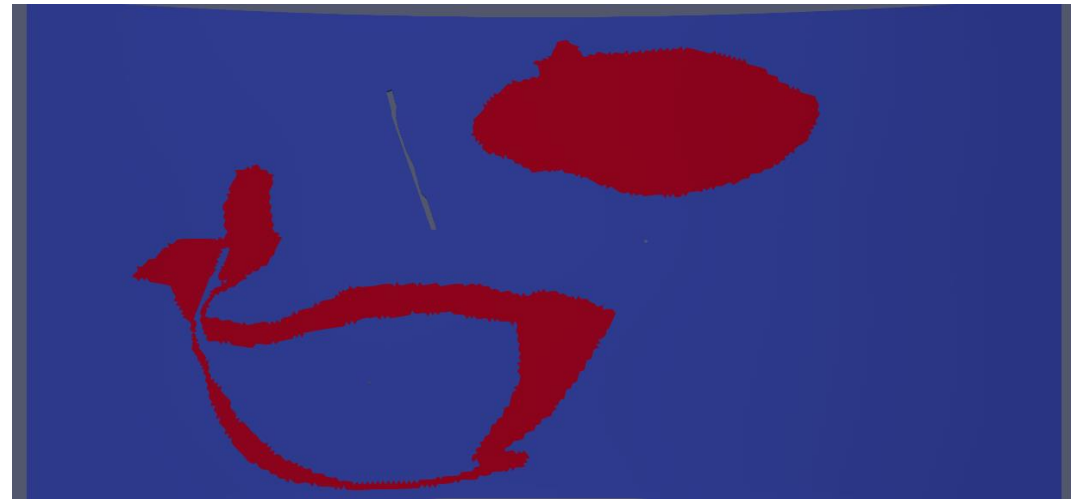
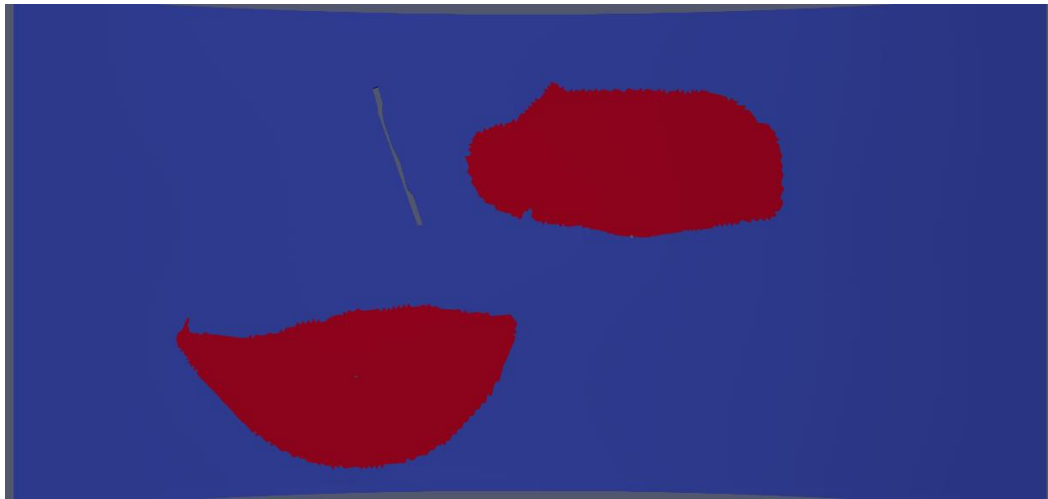
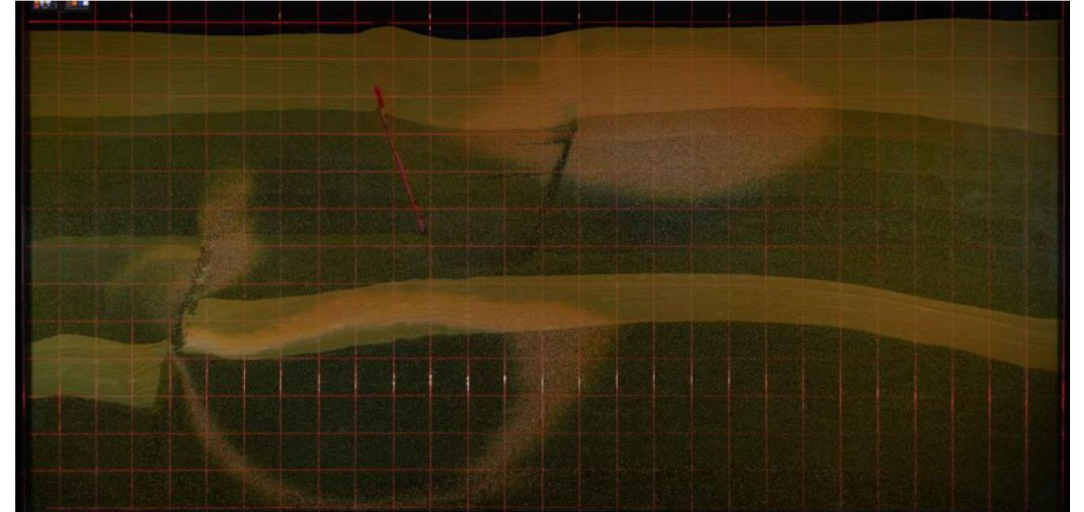
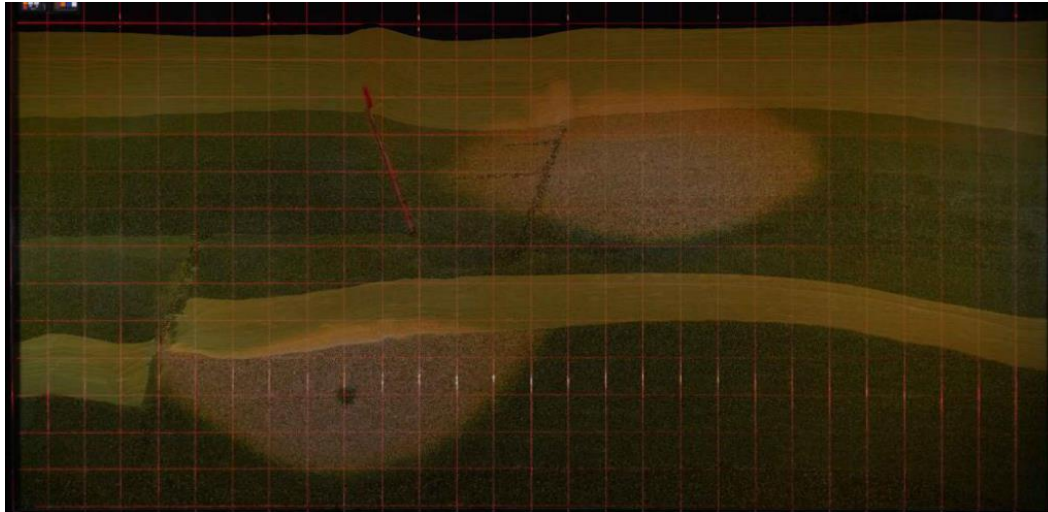
FluidFlower benchmark



Generation of prior realizations

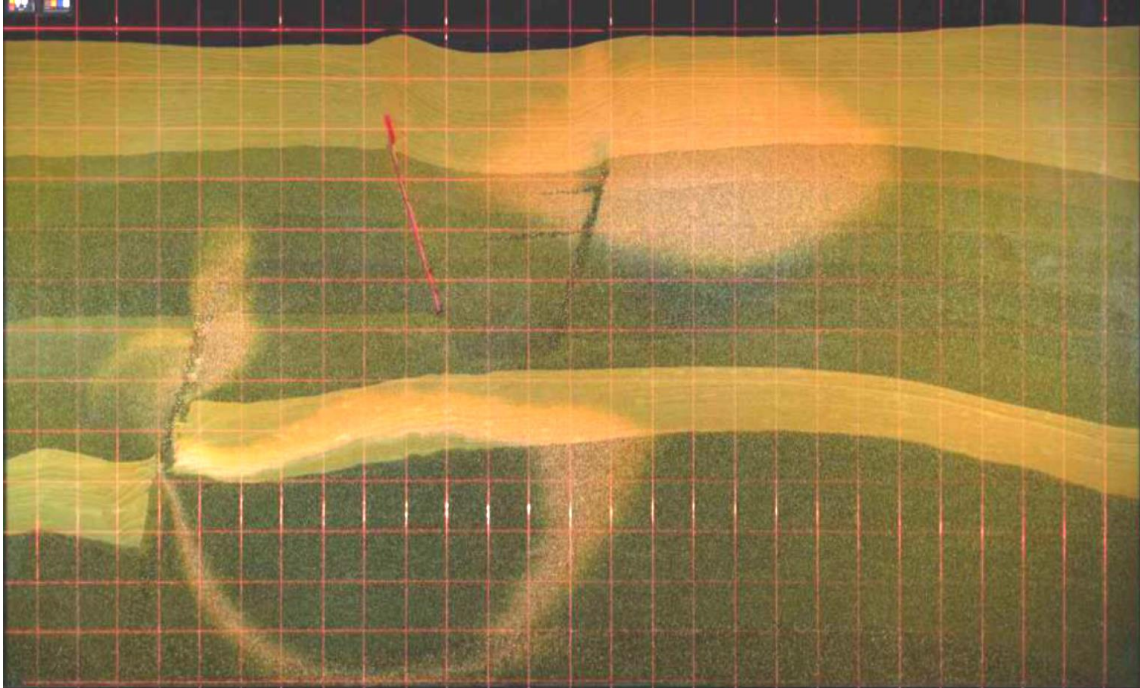


Digitizing of tracer test

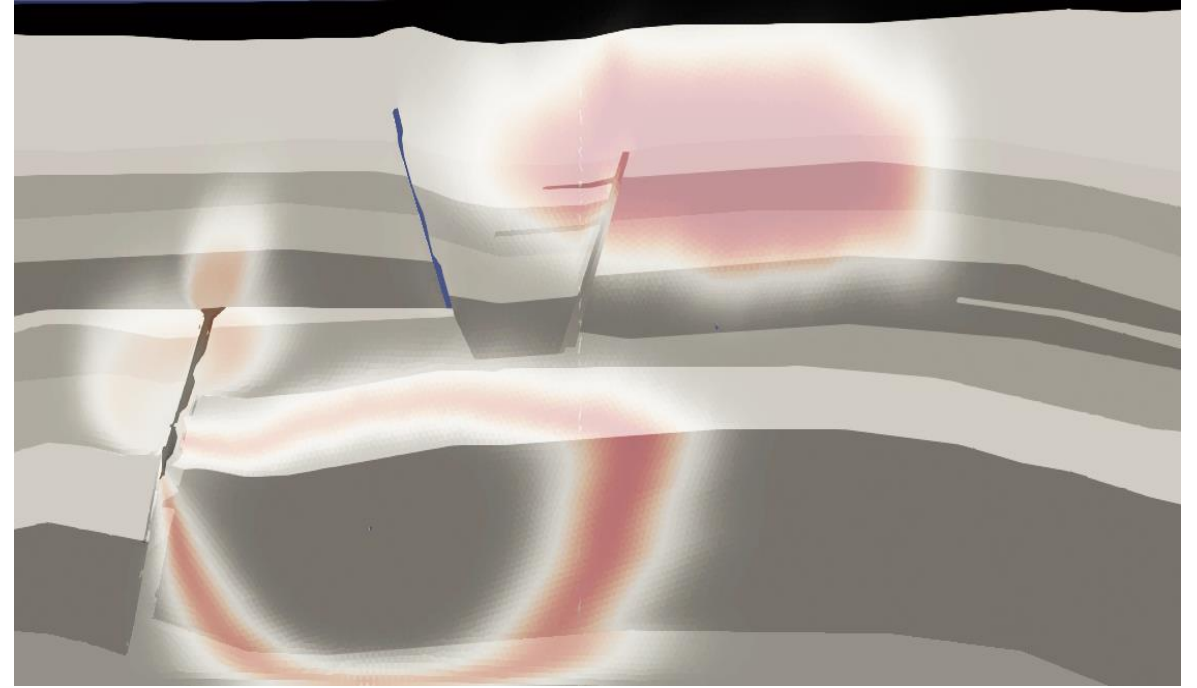


History matching using RML (single realization)

Tracer observations (high resolution images)



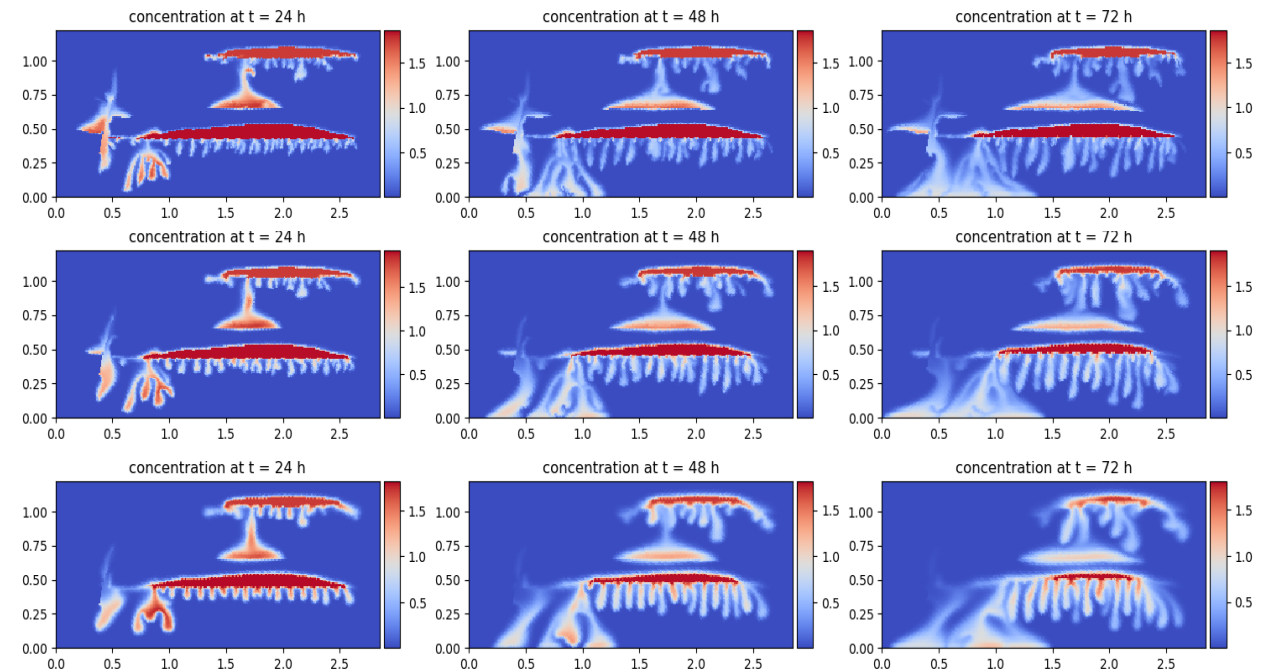
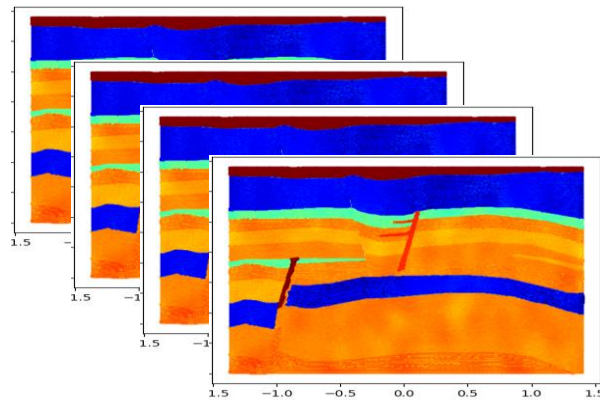
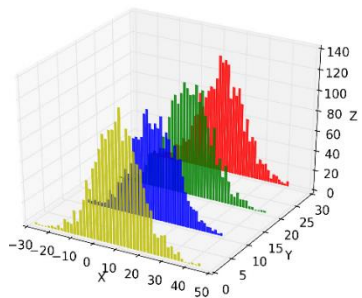
Inversed model (RML, 18,278 forward runs for 100 priors)



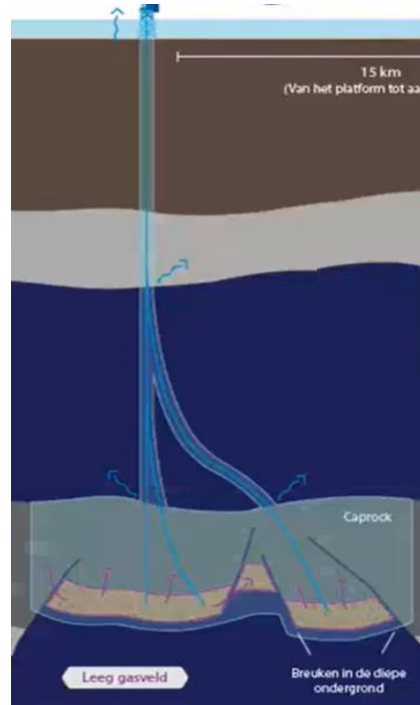
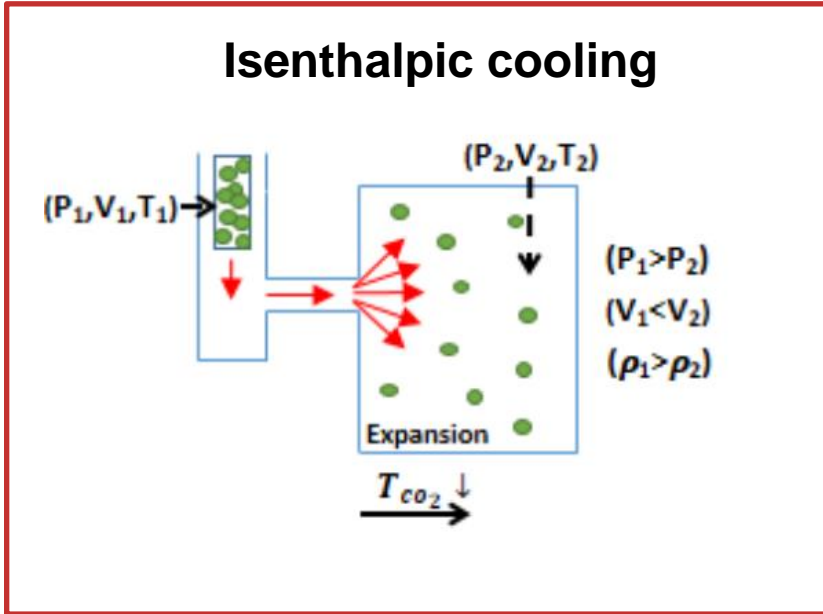
$$E(\mathbf{u}) = \frac{1}{2}(\mathbf{u} - \mathbf{u}_{\text{ref}})^T C_M^{-1}(\mathbf{u} - \mathbf{u}_{\text{ref}}) + \frac{1}{2}(G(\mathbf{u}) - \mathbf{d}_{\text{obs}} + \boldsymbol{\epsilon})^T C_D^{-1}(G(\mathbf{u}) - \mathbf{d}_{\text{obs}} + \boldsymbol{\epsilon})$$

Data Assimilation for FluidFlow experiments

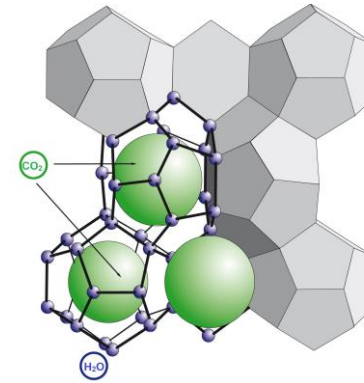
- Models: 100 history matched permeability maps
- Temperature: $23^{\circ}\text{C} \pm 2$, normal distribution
- Diffusion: $2 \cdot 10^{-10} - 2 \cdot 10^{-9}$, log-normal distribution
- Two phase: Corey parameters with std from 5 to 50%, normal distribution



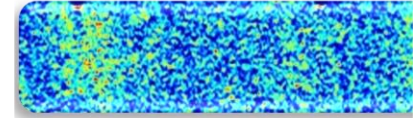
CCS in depleted fields: Joule-Thomson cooling



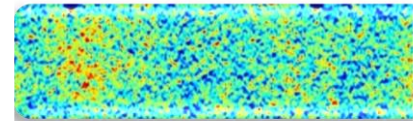
Hydrate formation



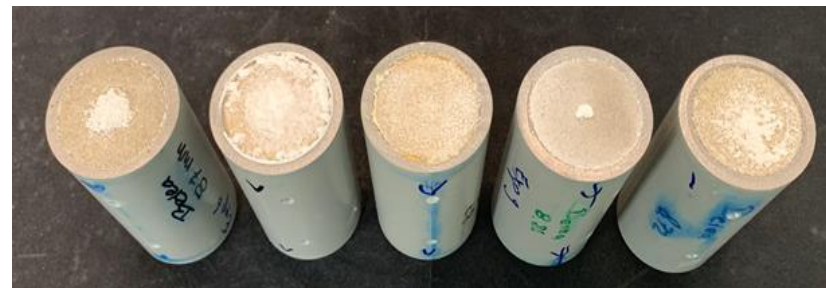
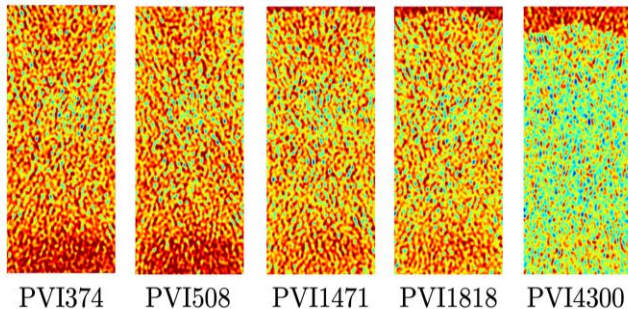
after hyd diss: W/CO₂



after hyd form: W/CO₂/H

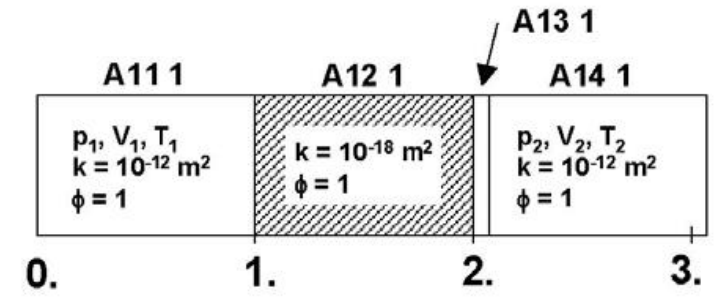
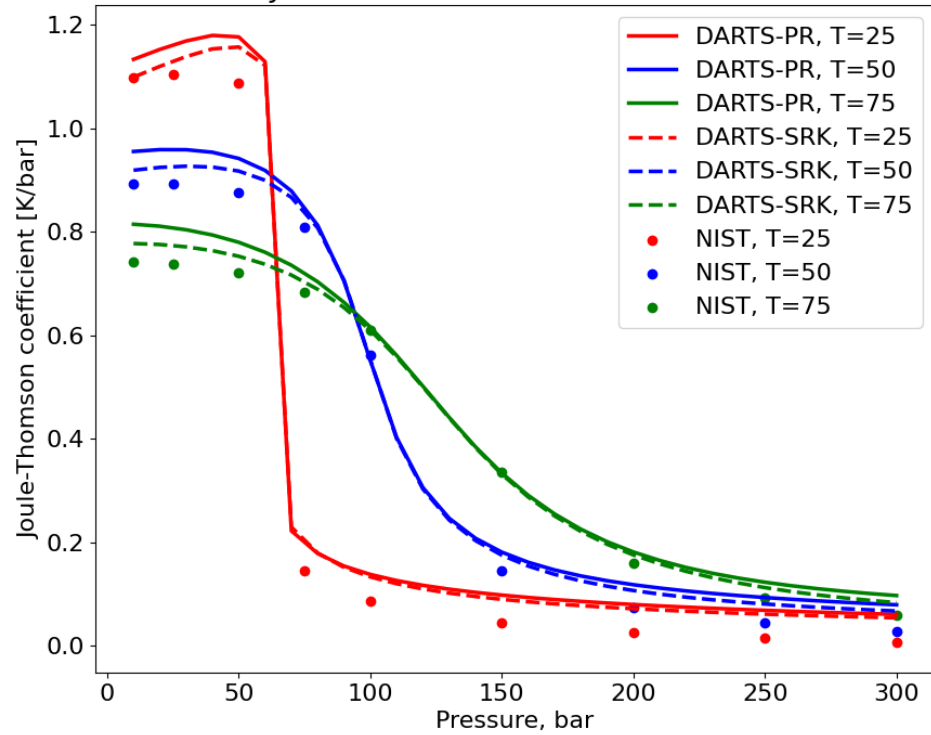


Salt precipitation



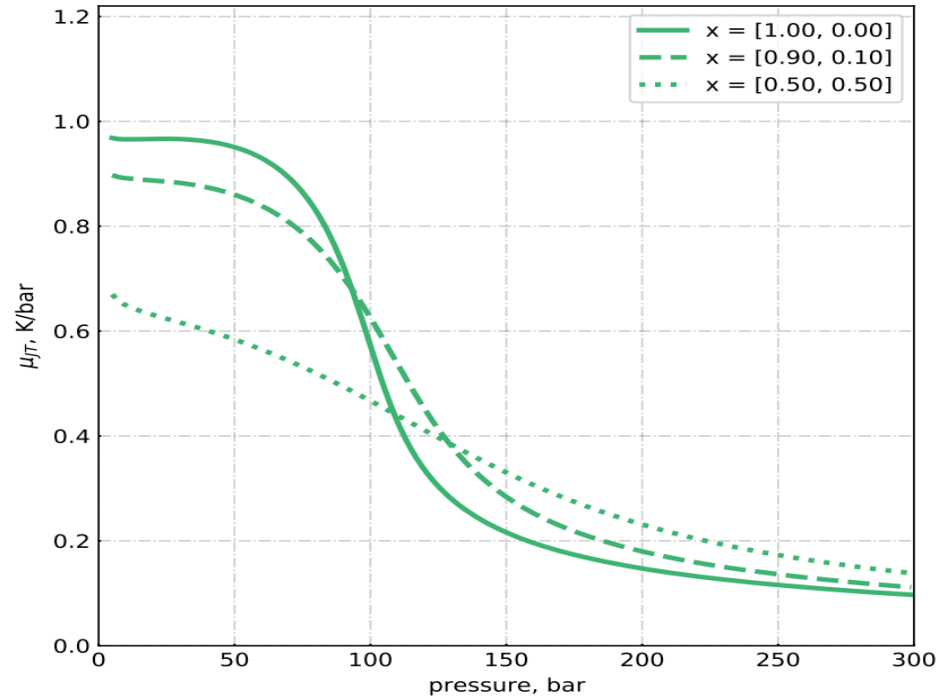
JT-cooling validation

Cooling for Pure CO₂



Oldenburg, 2006

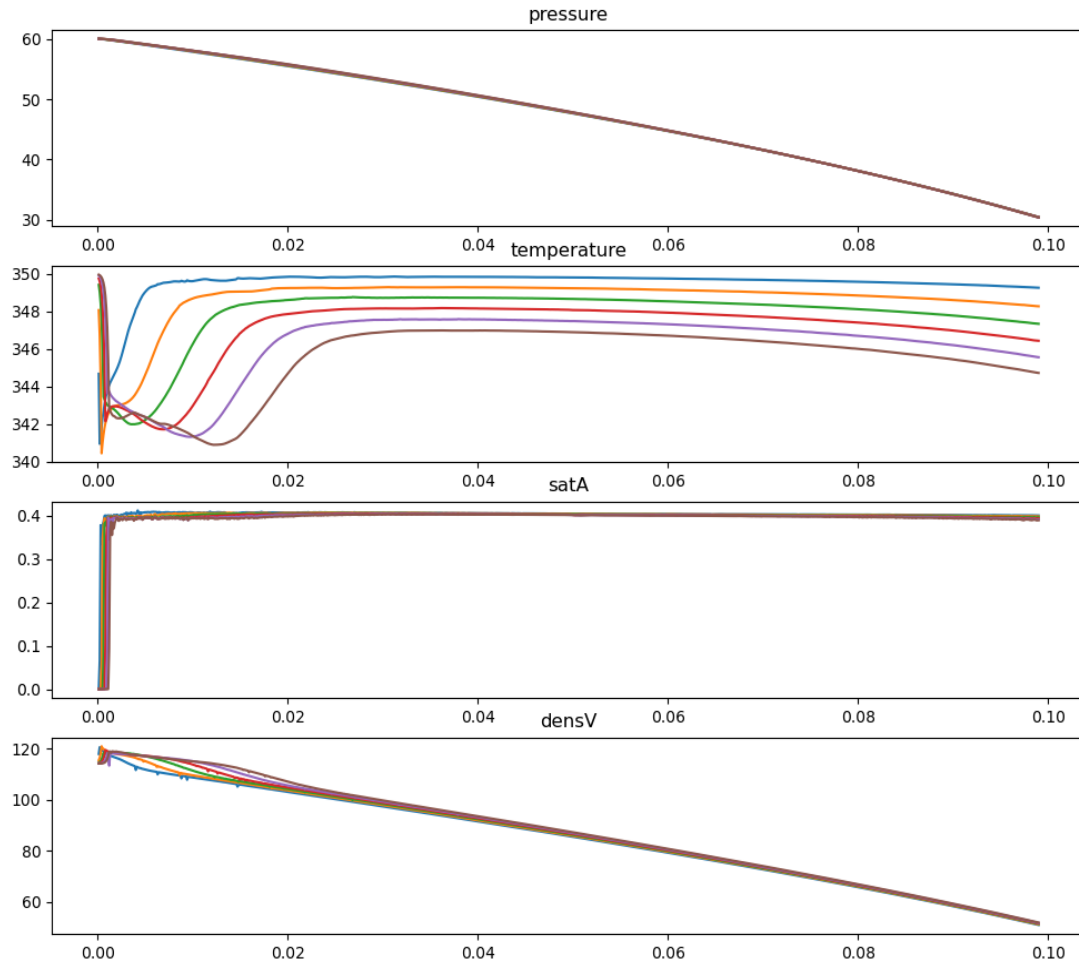
Cooling for Mixtures CO₂-CH₄



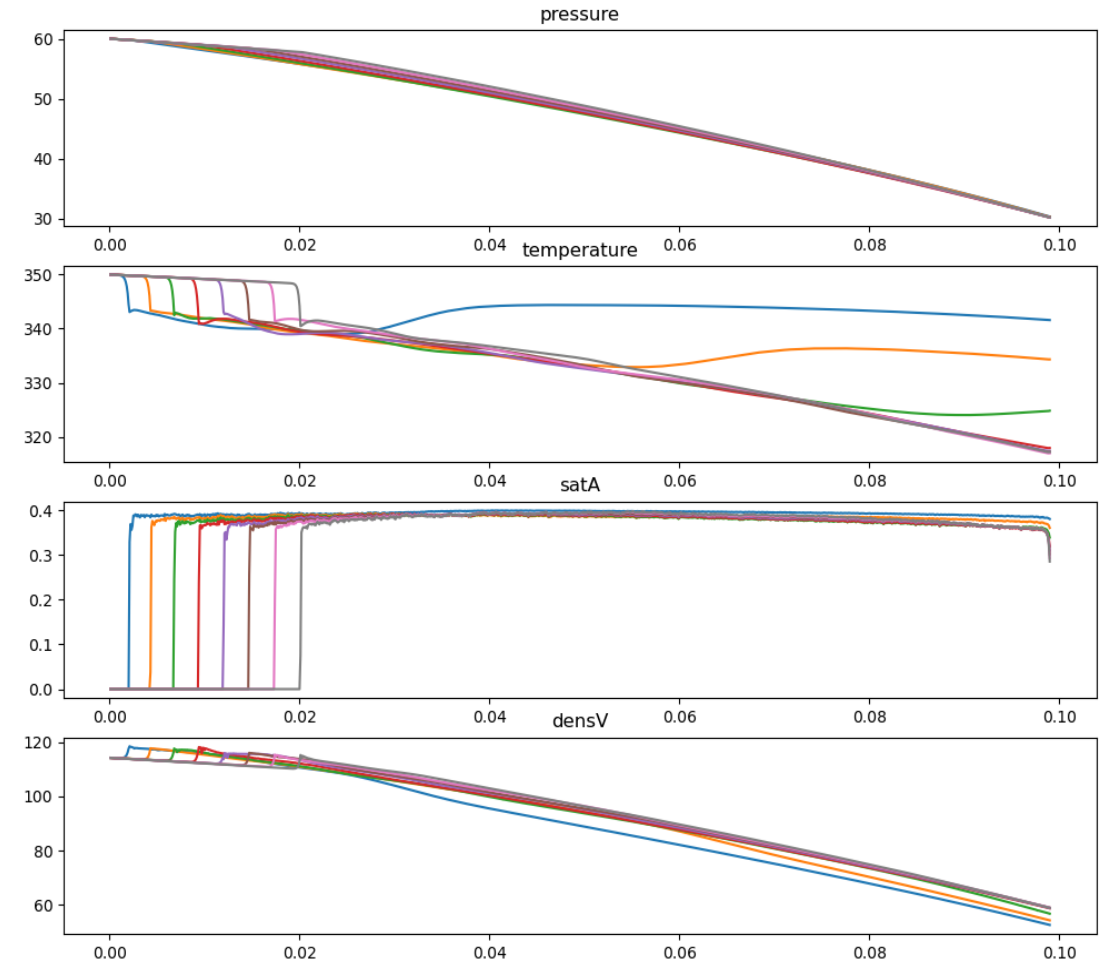
JT effect at various scales



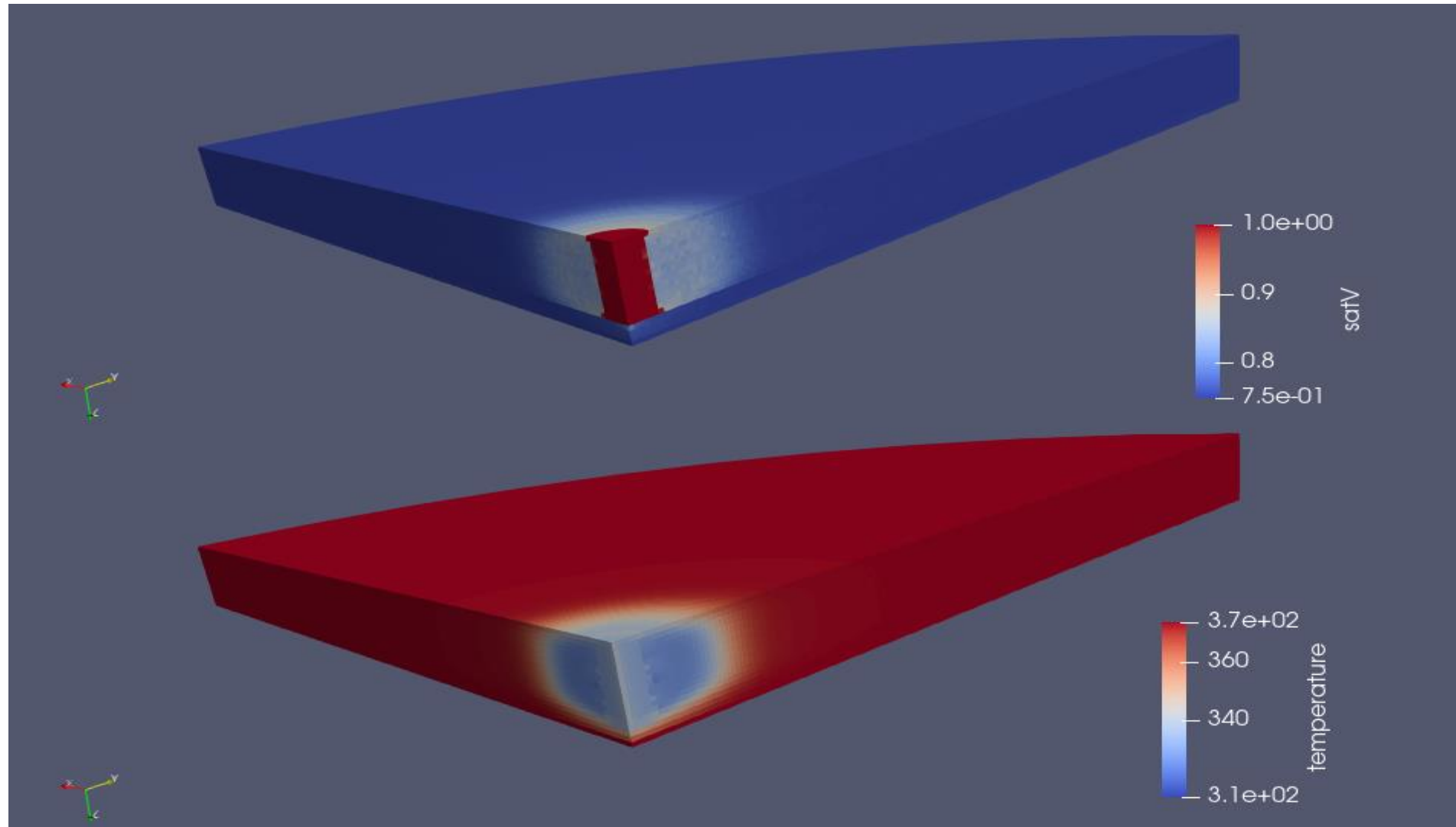
JT in CO₂-CH₄-H₂O system at experimental scale, 1 sec



JT in CO₂-CH₄-H₂O system at experimental scale, 10 sec

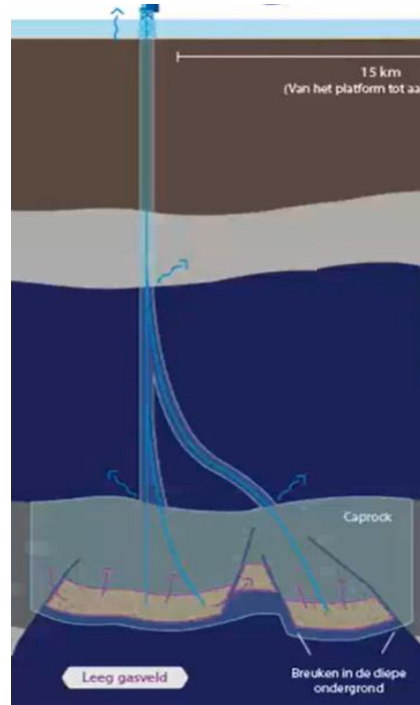
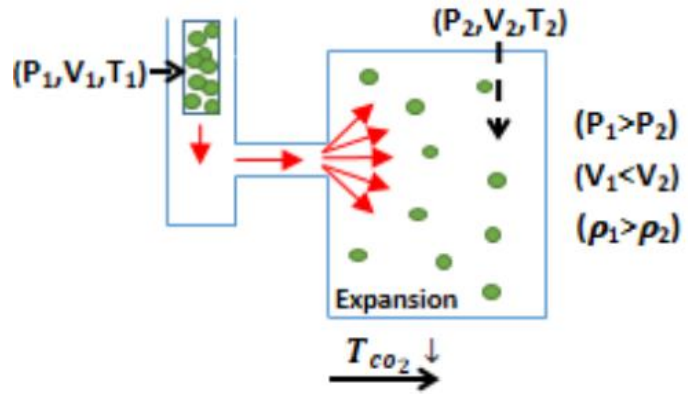


Radial model results

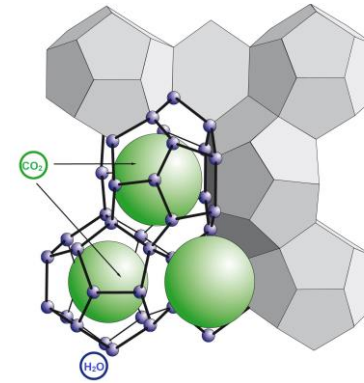


CCS in depleted fields: impact of salt precipitation

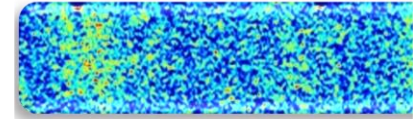
Ienthalpic cooling



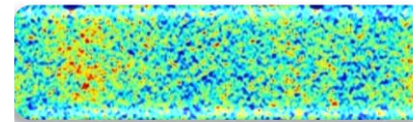
Hydrate formation



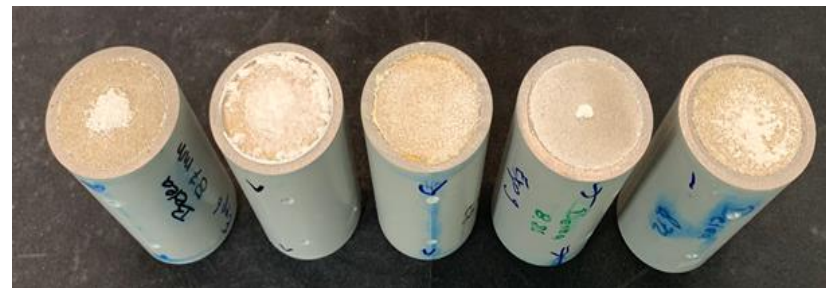
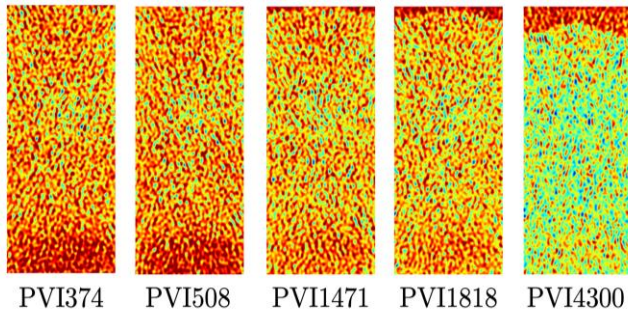
after hyd diss: W/CO₂



after hyd form: W/CO₂/H

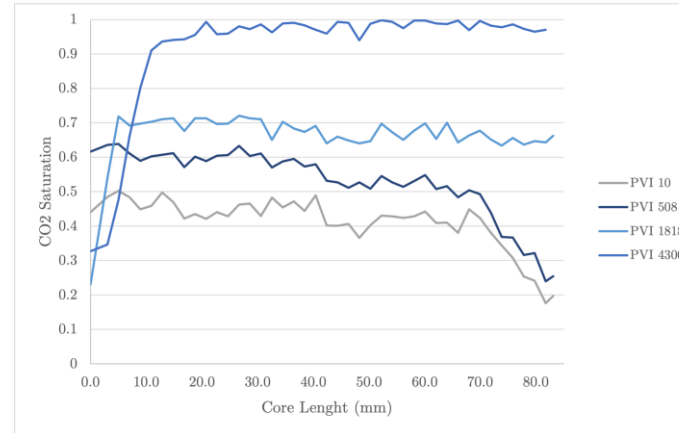
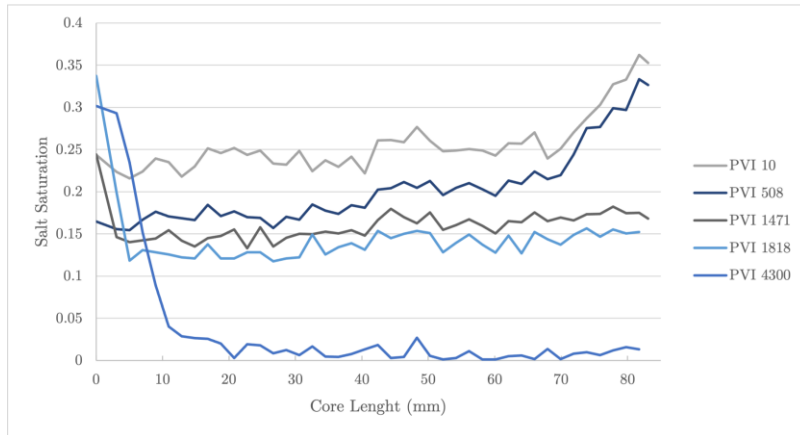


Salt precipitation



Salt precipitation: core flood experiments

Gas and salt saturations in a homogeneous core



3D reconstruction of salt in Bentheimer core

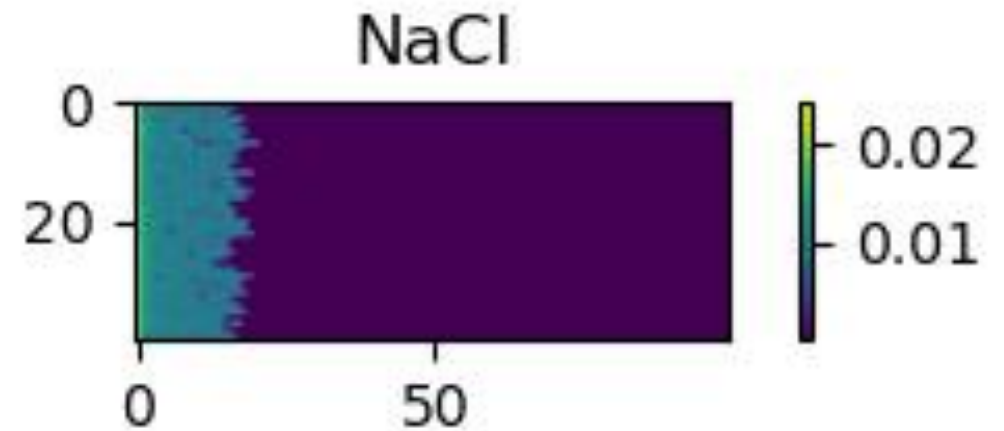
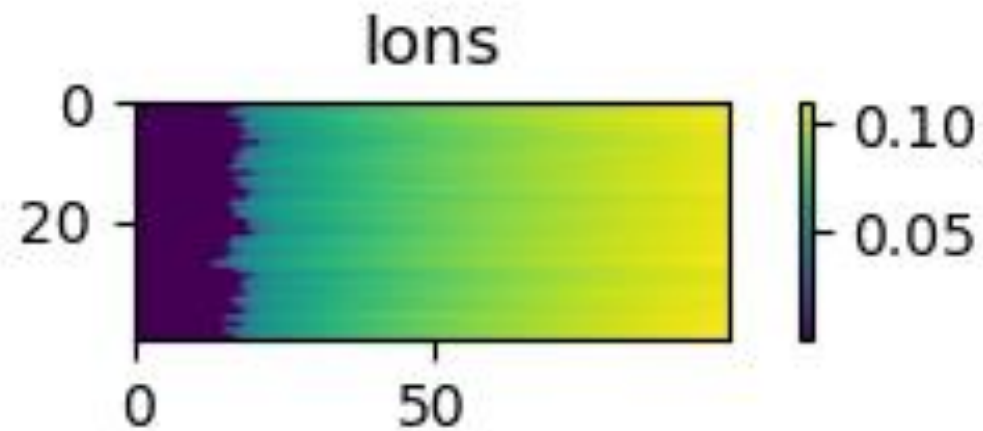
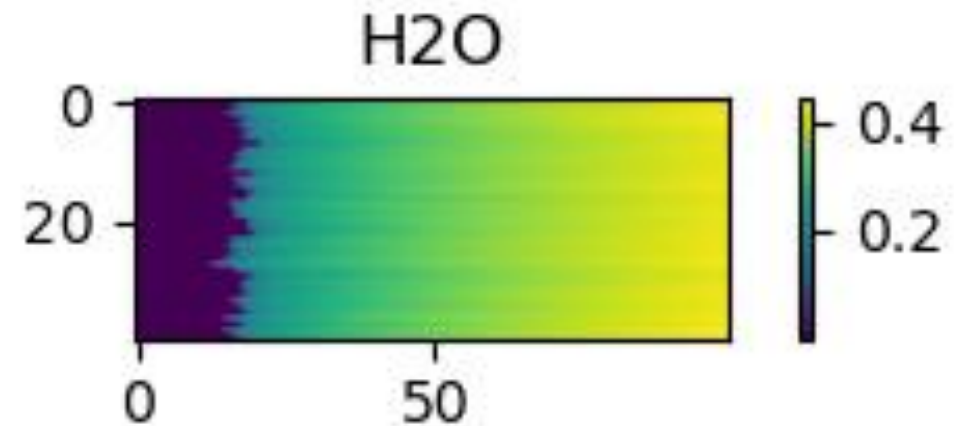
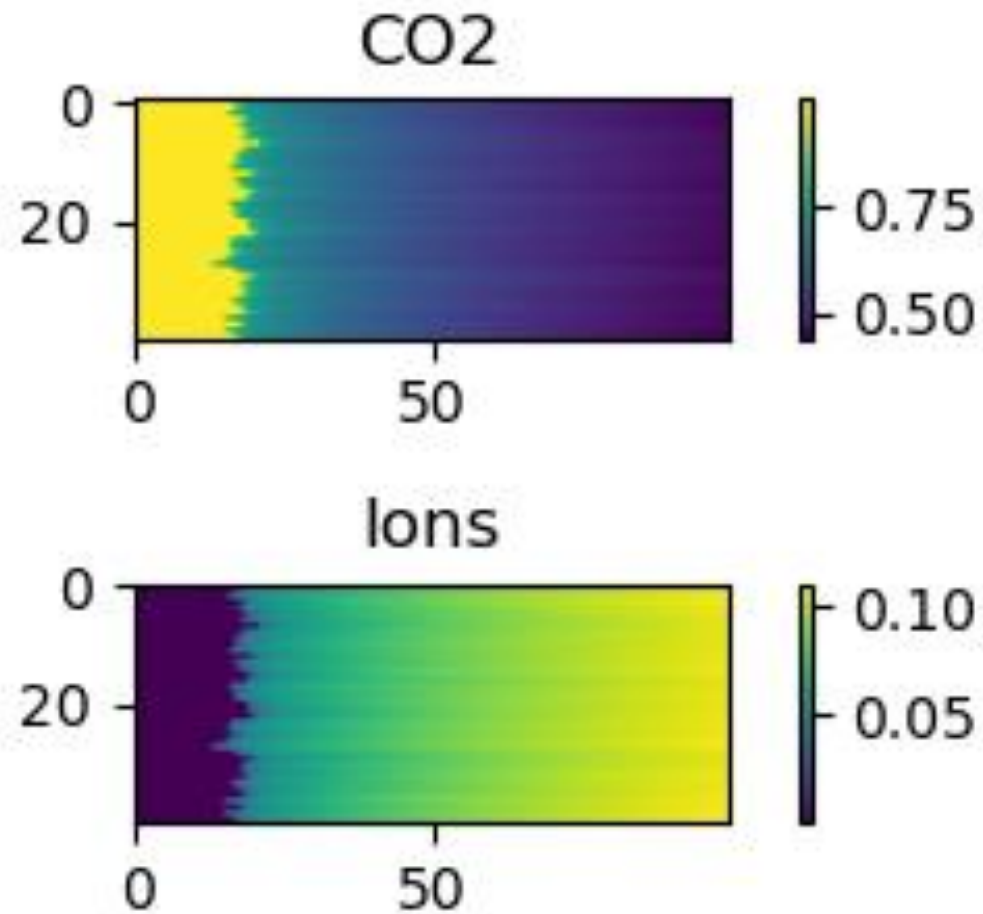


Permeability reduction in a homogeneous core

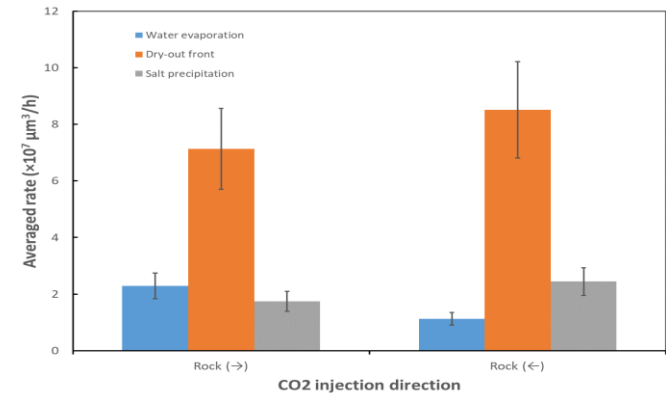
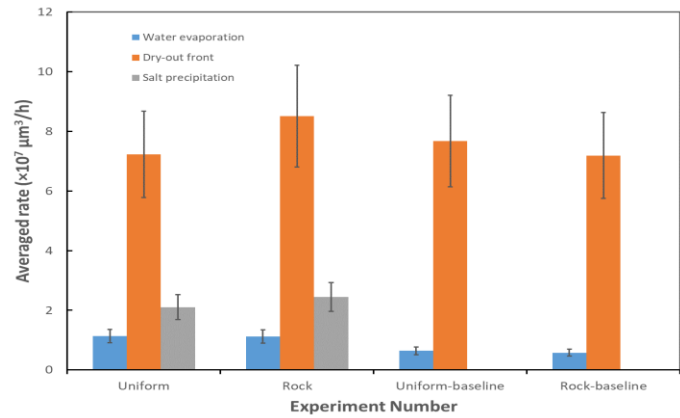
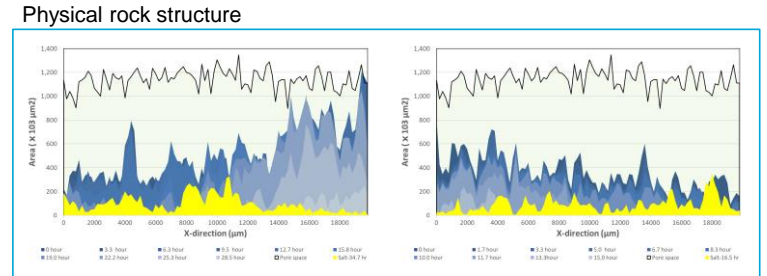
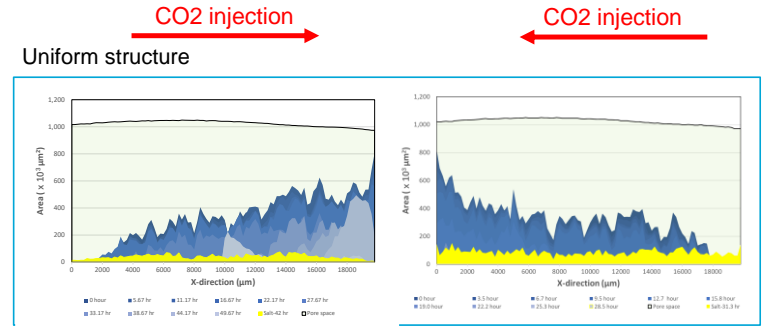
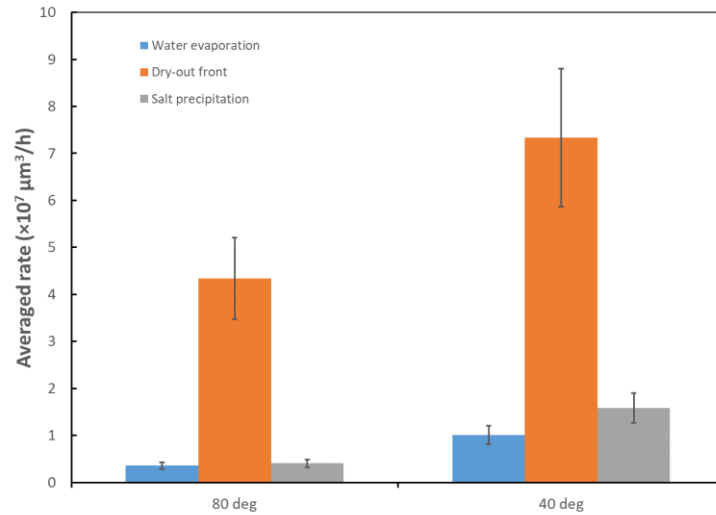
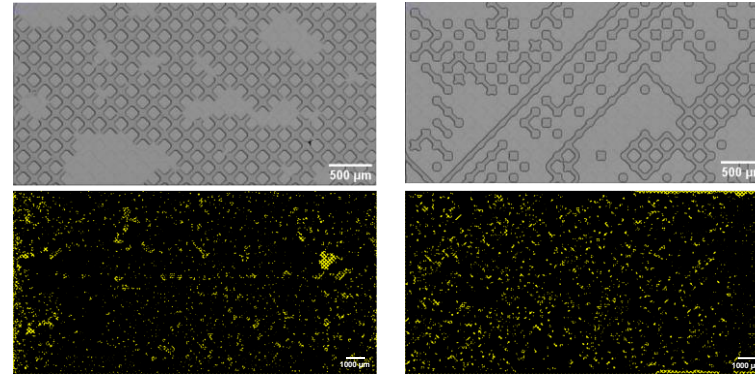
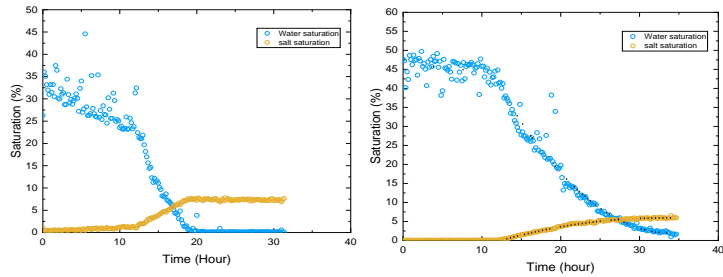
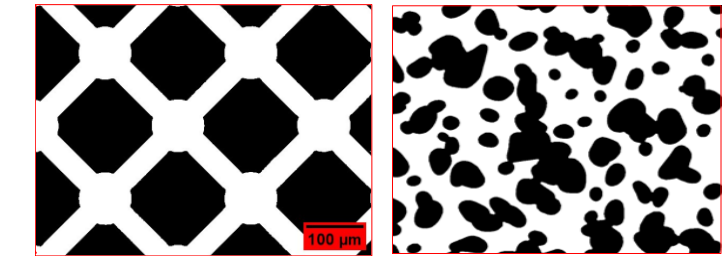
Core type	1st section of core			2nd section of core		
	K initial (mD)	K final (mD)	K reduction	K initial (mD)	K final (mD)	K reduction
Bentheimer	2164	24	99%	1707	170	90%
Berea	164	0.8	99%	168	148	12%
Fontainebleau	164	18	99%	187	170	9%

Salt mainly precipitated at inlet regions and permeability had a huge reduction in it

Simulation results with DARTS

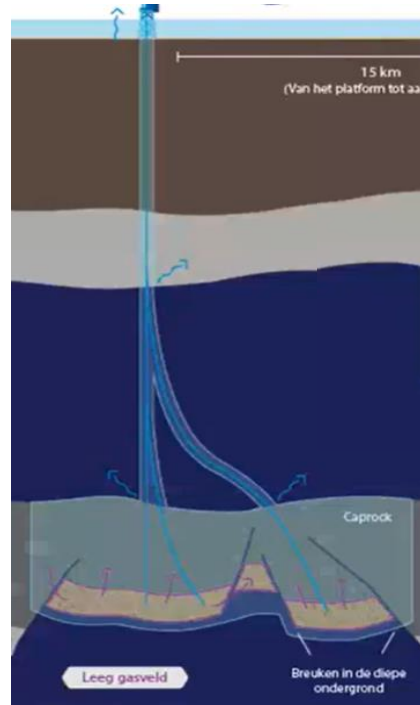
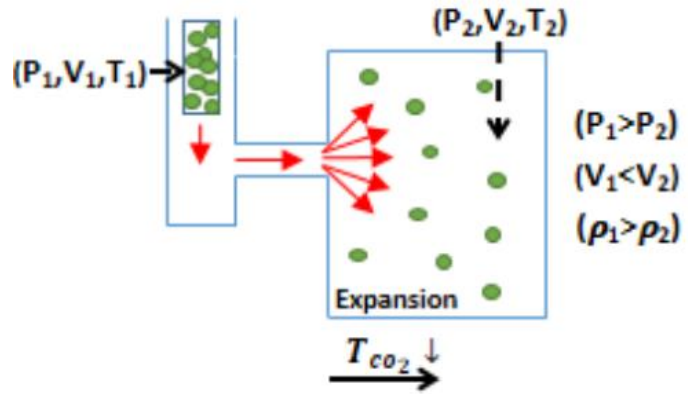


Impact of pore structure, wettability and direction

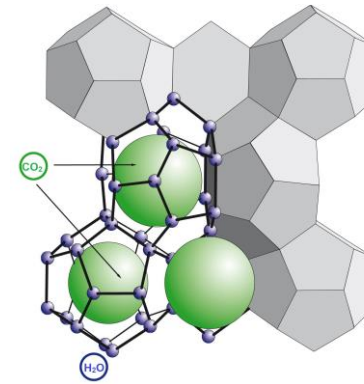


CCS in depleted fields: risk of hydrate formation

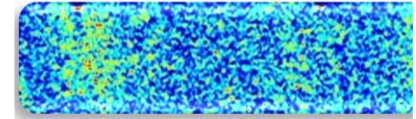
Isenthalpic cooling



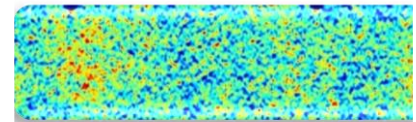
Hydrate formation



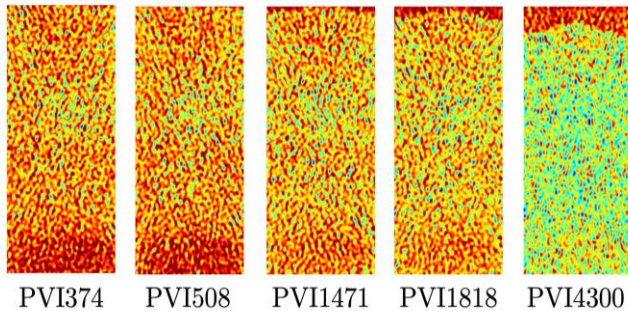
after hyd diss: W/CO₂



after hyd form: W/CO₂/H



Salt precipitation



Thermodynamic models for hydrates

- Van der Waals and Platteeuw (1958)
 - Chemical potential change upon cage filling

$$\frac{\Delta\mu_{w,H}}{RT} = \frac{\mu_{w,H}}{RT} - \frac{g_{w,\beta}}{RT} = \sum_m \nu_m \ln \left(1 - \sum_j \theta_{jm} \right)$$

- Fugacity related to reference phase

$$f_{w,H} = f_{w,A} \exp \left[\frac{\Delta\mu_{w,H} - \Delta\mu_{w,A}}{RT} \right]$$

- Langmuir 'adsorption'

$$\theta_{jm} = \frac{C_{jm} f_j}{1 + \sum_k C_{km} f_k}$$

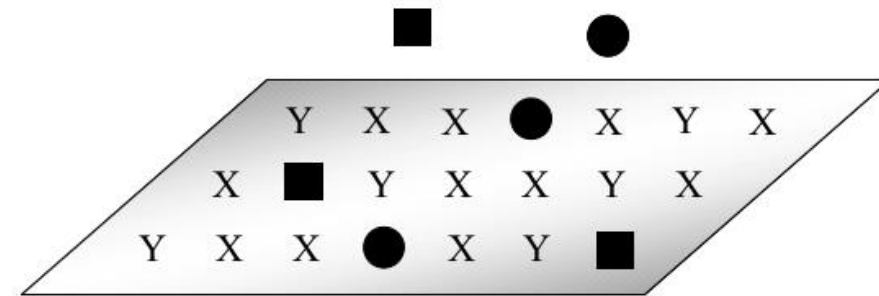
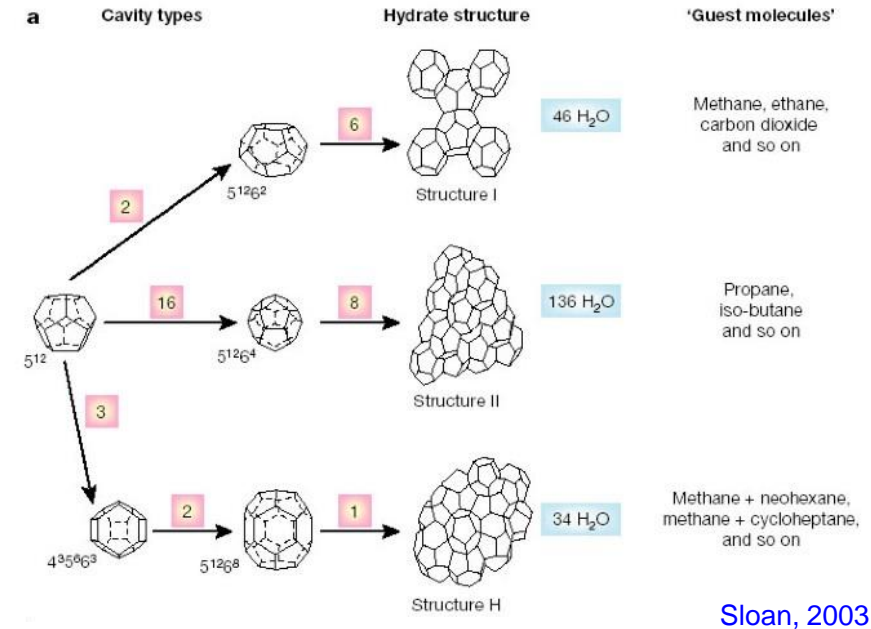
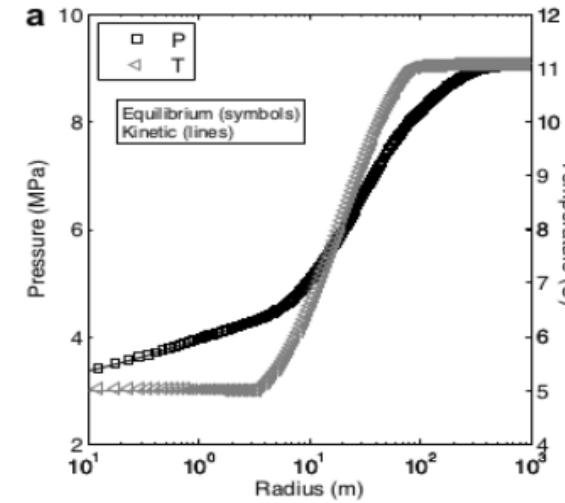


Figure 4.1 Visual of multi-site, multi-component adsorption

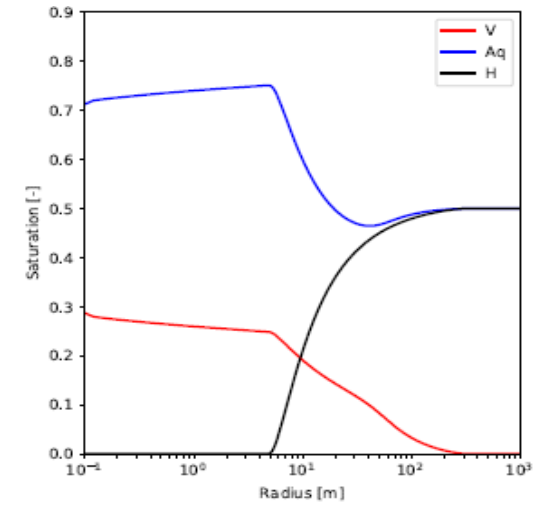
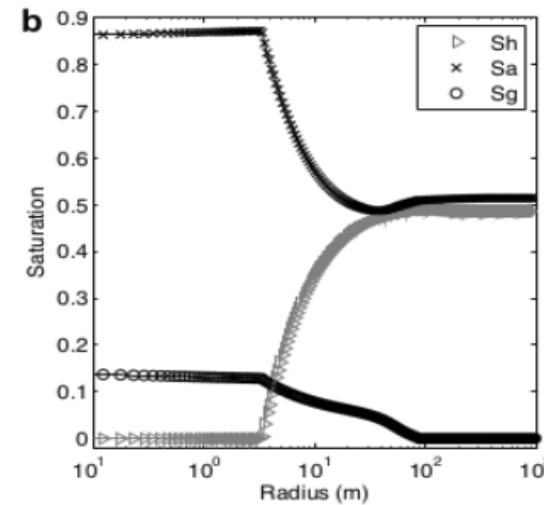
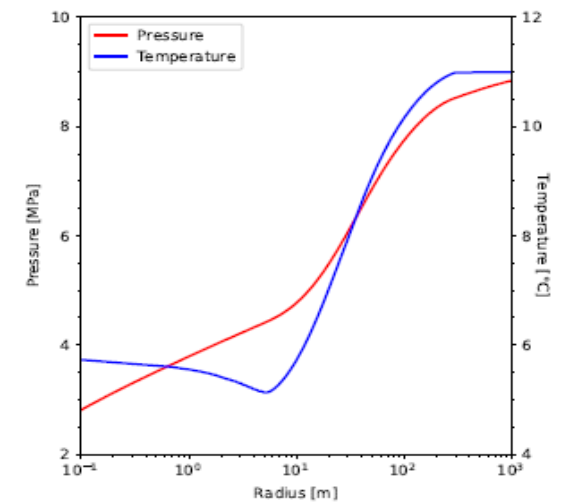
Hydrate dissociation

- Class 3 hydrate deposit
 - Radial reservoir
 - Partially saturated with CH₄-hydrate
 - Pressure at well 27 bar

TOUGH+Hydrate



DARTS



Kowalsky & Moridis, 2007

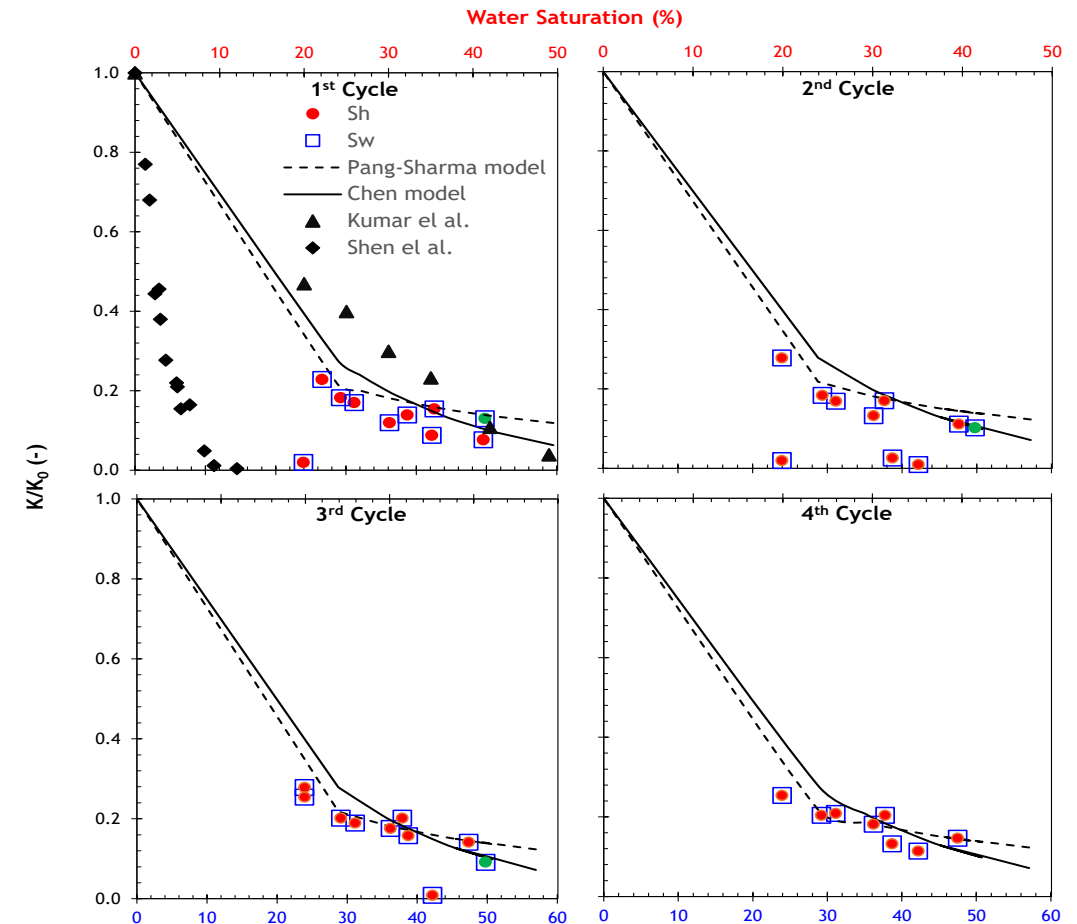
Wapperom & Voskov, in prep.

Impact of water saturation on permeability

Exp	Core	Salt type/concentration
1-9	Bentheimer	1wt% NaCl
10	Bentheimer	1wt% NaCl

Note: In exp 10, for the first 2 cycles, the normalized permeability was calculated based on the differential pressure, while for the third cycle brine permeability test was performed in the presence of hydrate to validate the previous calculation.

Permeability is directly influenced by hydrate saturation, which is, in turn, dependent on the water saturation level.



Aghajanloo et al., in prep.

Acknowledgments

- DARTS team: Mark Khait, Xiaocong Lyu, Yang Wang, Xiaoming Tian, Stephan de Hoop, Kiarash Mansour Pour, Artur Palha, Aleks Novikov, Michiel Wapperom, Yuan Chen, George Hadjisotiriou, Gabriel Serrao Seabra, Luisa Orozco
- ASSET team: Rouhi Farajzadeh, Mahnaz Aghajanloo, Lifei Yan, Michiel Slob, Sadegh Taghinejad, Manon Schellart, Georgios Ntentopoulos
- Students and colleagues: Dan Nichita, Juan Diego Heringer, Andrey Margert, Michel Kern, Brahim Amaziane, Jan Norbotten, Bernd Flemisch, James Gunning



open-DARTS



Time for Questions and Answers

